



STATE OF NORTH CAROLINA  
DEPARTMENT OF TRANSPORTATION

MICHAEL F. EASLEY  
GOVERNOR

LYNDO TIPPETT  
SECRETARY

August 11, 2004

U.S. Army Corps of Engineers  
Raleigh Regulatory Field Office  
6508 Falls of Neuse Road  
Suite 120  
Raleigh, NC 27615

ATTN: Mr. Eric Alsmeyer  
NCDOT Coordinator

Dear Sir:

SUBJECT: **Permit Modification Request for TIP No. R-2809B**, Wake County, NC  
DOT Division 5, Federal Aid No. STP-98(1), State Project No. 8.1402501,  
USACE Action ID 199601836, and DWQ Project No. 010550, \$475 Debit  
Work Order WBS Element 34503.1.1

On October 30, 2003 and October 22, 2003 respectively, the USACE 404 Individual Permit and the NCDWQ 401 Water Quality Certification and Neuse River Riparian Certification were issued for the subject project. The North Carolina Department of Transportation (NCDOT) proposes to modify the construction plans for the abovementioned project. The purpose of this letter is to request a modification to the Department of the Army Individual Permit, the 401 Water Quality Certification as well as the Buffer Certification from the NC Division of Water Quality. The revised sheets of the original permit drawings are attached.

**Summary of Impact Changes**

Revisions were made to the permit drawings in order to be consistent with the construction plans. Changes in impacts result from expanding the construction areas to allow sufficient access for equipment, realignment of a ramp, impacts due to the relocation of a stream and culvert extensions, decrease in impacts due to a third party having filled an UT to Richland Creek, and the contractor clearing a buffer outside of the permitted area.

Streams: Additional stream channel impacts total 358 feet of permanent impacts and 143 feet of temporary impacts. Onsite natural stream design increased by 351 ft.

Buffers: Buffer impacts have increased by 30,905ft<sup>2</sup>, allowable buffer impacts have decreased by 13,874ft<sup>2</sup> and mitigable buffer impacts have increased by 44,779ft<sup>2</sup>. Onsite Buffer replacement will increase by 45,616ft<sup>2</sup> at Site 4. Specific revisions are summarized in Table 1 and Table 2 and are listed below, site by site. Site numbers correspond to the original permit drawing sheets. Sheet numbers also correspond to the original permit drawings with a date that the drawing has been revised.

<b>Table 1: Permanent Jurisdictional Stream Impact Changes</b>				
Site #	Station #	Original Impacts	Revised Impacts	Increase
1	-L- 31+96 / -Y2- 11+38	790	797	7
4	-L- 37+74L / 38+34L	0	351	351
<b>Total</b>				<b>358</b>

<b>Table 2: Buffer Impact Changes (Mitigatable and Allowable)</b>				
Site #	Station #	Original Impacts (sq. ft.)	Revised Impacts (sq. ft.)	Increase (sq. ft.)
1	-L- 31+96/ -Y2-11+38	68747	72127	3380
2	-Y2- 10+42L/-Y2- 10+89L	7484	14036	6552
3	-Y1 16+88L/-RPB- 11+01L	14981	19449	4468
3	-Y1- 16+98R/17+70R	5370	10150	4780
4	-Y3-10+77R/11+05R	23847	2476	-21371
4	-L-38+24.5/39+44.5	17674	46466	28792
4	-L- 40+00 L	0	1324	1324
5	-L- 47+09L/47+70R	27287	30267	2980
<b>Totals</b>		<b>165,390</b>	<b>196,295</b>	<b>30,905</b>

The revised design does not compromise NCDOT's compliance with the existing permit conditions. The new impact sites have been evaluated for compliance with the avoidance/minimization criteria and are in compliance with all previous Individual Permit factors, including the following:

- Protected Species,
- Cultural Resources,
- Aquatic Life passage,
- FEMA compliance, and
- Utilities.

#### **REVISIONS RESULTING IN 404 and 401 JURISDICTIONAL CHANGES**

##### **Site 1, Sheet 4 of 26**

Station -L-31+96

The impacts to the stream were previously calculated by measuring to the end of the rip rap and are now calculated by measuring to the edge of the Right-of-way.

**Impact change: increase of 7 ft of permanent Stream Impacts**

Site 4, Sheets 17 and 18 of 26

Station -L-38+84

The original survey of Richland Creek was inaccurate and did not take into account a bend to the west. The project was originally designed so that all bents would not be placed in Richland Creek. However, due to the inaccuracy of the survey, piers 1 and 2 of the bent 2 would fall in the stream. An onsite field meeting was held on June 17 between NCDOT officials, USACE and NCDWQ. During the meeting it was agreed that the banks of Richland Creek were not stable and that Richland Creek could be relocated using natural stream design. Approximately 351 feet of Richland Creek will be relocated. Due to the limited amount of space between the bents and an existing below ground sewer line the relocation of Richland Creek will require two phases of temporary diversion channels. The sequencing of the stream relocation is as follows:

- Isolate diversion (secondary diversion) with dikes
- Dig diversion (secondary diversion)
- Install dikes in Richland Creek around proposed piers 1 and 2 and take out dikes isolating temporary secondary diversion
- Drill and install piers 1 and 2
- Construct main diversion, establish vegetation and reroute water
- Construct stream relocation, establish vegetation and reroute water

**Impact change: increase of 351 ft of permanent Stream Impacts**

**Increase of 351 ft of Natural Stream Design**

Increase of 82 feet of temporary Stream Impacts

Site 5, Sheet 21 of 26

Station -L-47+09L / 47+70R

The entire temporary drainage easement will be required to allow equipment access so that the contractor has sufficient room to install the culvert.

**Impact change: increase of 61 ft of temporary Stream Impacts**

**REVISIONS RESULTING IN BUFFER CHANGES**

Site 1, Sheet 4 of 20

Station -L- 31+96/ Y2- 11+38

The entire temporary drainage easement north of the proposed road will be required to allow equipment access for the placement of the pipes in the stream.

**Impact change: increase of 3,380 ft<sup>2</sup> of Mitigable Buffer Impacts**

Site 2, Sheet 5 of 20

Station -Y2- 10+42L / -Y2- 10 +89L

Additional area is required to allow equipment access for construction of stream relocation and to allow for a larger bankfull bench in the natural stream design. NCDOT requested prior approval because construction had already begun at this site and waiting on written approval would require the NCDOT to pay the contractor to go back and construct the stream relocation twice. These impacts were verbally authorized by John Hennessy on May 7, 2004.

**Impact change: increase of 6,552 ft<sup>2</sup> of Mitigable Buffer Impacts**

Site 3, Sheet 6 of 20

Station -Y1- 16+88L/ -RPB- 11+01L

Station -Y1- 16+98R/ 17+70R

The entire temporary drainage easement will be required to allow equipment access for the construction of the bridge.

**Impact change: increase of 9,248 ft<sup>2</sup> of Mitigable Buffer Impacts**

Site 4, Sheet 7, 8 and 9 of 20

Station -Y3- 10+84R/ 11+05 R

A portion of the stream at this location has been filled by Lowe's. Impacts incurred by NCDOT at this site have decreased from 23,847ft<sup>2</sup> to 2,467ft<sup>2</sup>. The buffer replacement of 7,045ft<sup>2</sup> cannot be accomplished since the stream has been filled. Buffer impacts are now below the 1/3 acre threshold and impacts are now considered "allowable" at this site.

**Impact change: decrease of 21,371ft<sup>2</sup> of Buffer Impacts/ decrease of 23,847ft<sup>2</sup> of Mitigable Impacts**

Station -L- 38+24.5/ 39+44.5

The contractor cleared outside of the permitted impact area. The ramp has also been realigned to allow for a grade change.

**Impact change: increase of 28,792ft<sup>2</sup> of Mitigable Buffer Impacts  
increase of 45,616ft<sup>2</sup> of Buffer Replacement**

Station -40+00 L

The Permanent Drainage Easement area was extended to allow access for equipment to build the Extended Dry Detention Basin and to allow future maintenance.

**Impact change: increase of 1,324ft<sup>2</sup> of Allowable Buffer Impacts**

Site 5, Sheet 10 of 20

Station -L- 47 + 09L/ 47 + 70R

The entire temporary drainage easement will be required to allow equipment access for the placement of the pipes in the stream.

**Impact change: increase of 2,980 ft<sup>2</sup> of Mitigable Buffer Impacts**

**Mitigation Strategy**

Based upon the agreements stipulated in the "Memorandum of Agreement Among the North Carolina Department of Environment and Natural Resources, the North Carolina Department of Transportation, and the U.S. Army Corps of Engineers, Wilmington District" (MOA), it is understood that the North Carolina Department of Environment and Natural Resources Ecosystem Enhancement Program (EEP), will assume responsibility for satisfying the federal Clean Water Act compensatory mitigation requirements for NCDOT projects that are listed in Exhibit 1 of the subject MOA during the EEP transition period which ends on June 30, 2005.

Since the subject project is listed in Exhibit 1, the necessary compensatory mitigation to offset unavoidable impacts to waters that are jurisdictional under the federal Clean Water Act will be provided by the EEP. The offsetting mitigation will derive from an inventory

of assets already in existence within the same 8-digit cataloguing unit. The Department has avoided and minimized impacts to jurisdictional resources to the greatest extent possible as described above.

Streams: The increase in permanent stream impacts total 358 feet; 351 feet will be mitigated on site via Natural Stream Design at Site 4. The remaining, unavoidable impacts to seven (7) feet of jurisdictional streams will be offset by compensatory mitigation provided by the EEP program. The NCDOT request letter to EEP is attached.

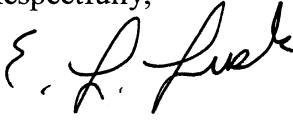
Buffers: No additional mitigation to Neuse River Buffer Areas is proposed because the increase in onsite buffer replacement (45,616f sqft.) offsets the increase in mitigable buffer impacts (44,779 sqft).

#### **Regulatory Approval**

The NCDOT respectfully requests that the referenced 404 Permit, 401 Water Quality Certification, and Neuse River Riparian Certification be modified to reflect the revisions outlined in this letter. In compliance with Section 143-215.3D(e) of the NCAC we will provide \$475 to act as payment for processing the Section 401 permit application previously noted in this application (see Subject line).

If you have any questions or need additional information, please contact Brett Feulner at (919) 715-1488.

Respectfully,

  
fcv  
Gregory J. Thorpe, Ph.D.  
Environmental Management Director, PDEA

Cc:

Mr. David Franklin, COE, Wilmington (Cover Letter only)	Mr. Greg Perfetti, P.E., Structure Design
Mr. John Hennessy, DWQ (7 copies)	Mr. Mark Staley, Roadside Environmental
Mr. Travis Wilson, NCWRC	Mr. Art McMillan, P.E., Highway Design
Mr. A.W. Roper, P.E., Div. 4 Engineer	Mr. Bill Gilmore, NC EEP
Ms. Becky Fox, EPA	Mr. Jamie Shern, DEO, Div 4
Mr. Ronald Mikulak, EPA	Mr. James Bridges, PDEA
Mr. Gary Jordan, USFWS	Mr. David Chang, P.E., Hydraulics
Mr. John Sullivan III, P.E., FHWA	Mr. Jay Bennett, P.E., Roadway
Mr. Omar Sullivan, P.E., Prog. Develop.	

File: R-2809B



STATE OF NORTH CAROLINA  
DEPARTMENT OF TRANSPORTATION

MICHAEL F. EASLEY  
GOVERNOR

LYNDO TIPPETT  
SECRETARY

August 11, 2004

Mr. William D. Gilmore, P.E.  
EEP Transition Manager  
Ecosystem Enhancement Program  
1652 Mail Service Center  
Raleigh, NC 27699-1652

Dear Mr. Gilmore:

Subject: **Revised Mitigation Request**, Wake Forest Bypass, Wake County, Federal Project No. STP-98(1), State Project No. 81402501, TIP No. R-2809B.

The purpose of this letter is to request that the North Carolina Ecosystem Enhancement Program (EEP) provide confirmation that the EEP is willing to provide compensatory mitigation for the project in accordance with the Memorandum of Agreement (MOA) signed July 22, 2003 by the USACE, the NCDENR and the NCDOT.

The North Carolina Department of Transportation has begun the construction of the Wake Forest Bypass. Jurisdictional impacts on this project have increased since the original permits were received and occur in the Neuse River Basin. NC WRP committed to provide mitigation for the impacts previously permitted. This project is on the list of projects covered by EEP.

**RESOURCES UNDER THE JURISDICTION OF SECTION 404 AND 401 OF THE CLEAN WATER ACT.**

We have avoided and minimized the impacts to jurisdictional resources to the greatest extent possible as described in the permit application. A copy of the permit application can be found at <http://www.ncdot.org/planning/pe/naturalunit/Applications.html>. The remaining impacts to jurisdictional resources will be compensated for by mitigation provided by the EEP program.

The project is located in the Piedmont Physiographic Province in Wake County in the Neuse River basin in Hydrological Cataloguing Unit 03020201.

- The stream impacts requiring offsite mitigation have increased by 7 feet.

**MAILING ADDRESS:**  
NC DEPARTMENT OF TRANSPORTATION  
PROJECT DEVELOPMENT AND ENVIRONMENTAL ANALYSIS  
1548 MAIL SERVICE CENTER  
RALEIGH NC 27699-1548

TELEPHONE: 919-733-3141  
FAX: 919-733-9794  
WEBSITE: [WWW.DOH.DOT.STATE.NC.US](http://WWW.DOH.DOT.STATE.NC.US)

**LOCATION:**  
TRANSPORTATION BUILDING  
1 SOUTH WILMINGTON STREET  
RALEIGH NC

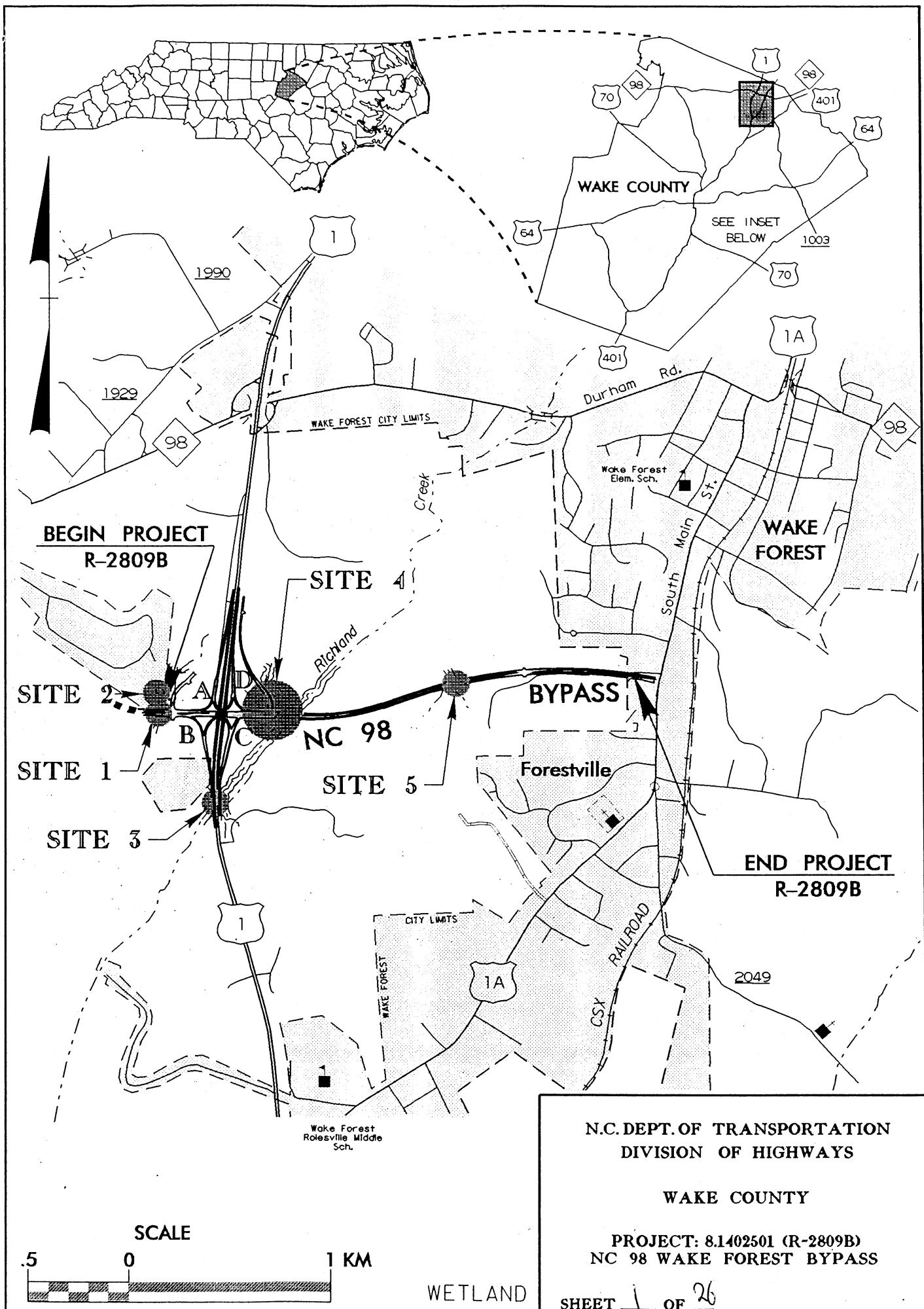
Please send the letter of confirmation to Eric Alsmeyer (USACE Coordinator) at U. S. Army Corps of Engineers Raleigh Regulatory Field Office, (6508 Falls of the Neuse Road/ Suite 120, Raleigh, NC, 27615). Mr. Alsmeyer's FAX number is 876-5823. This project is currently under construction.

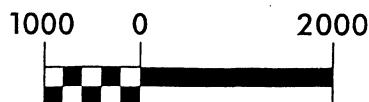
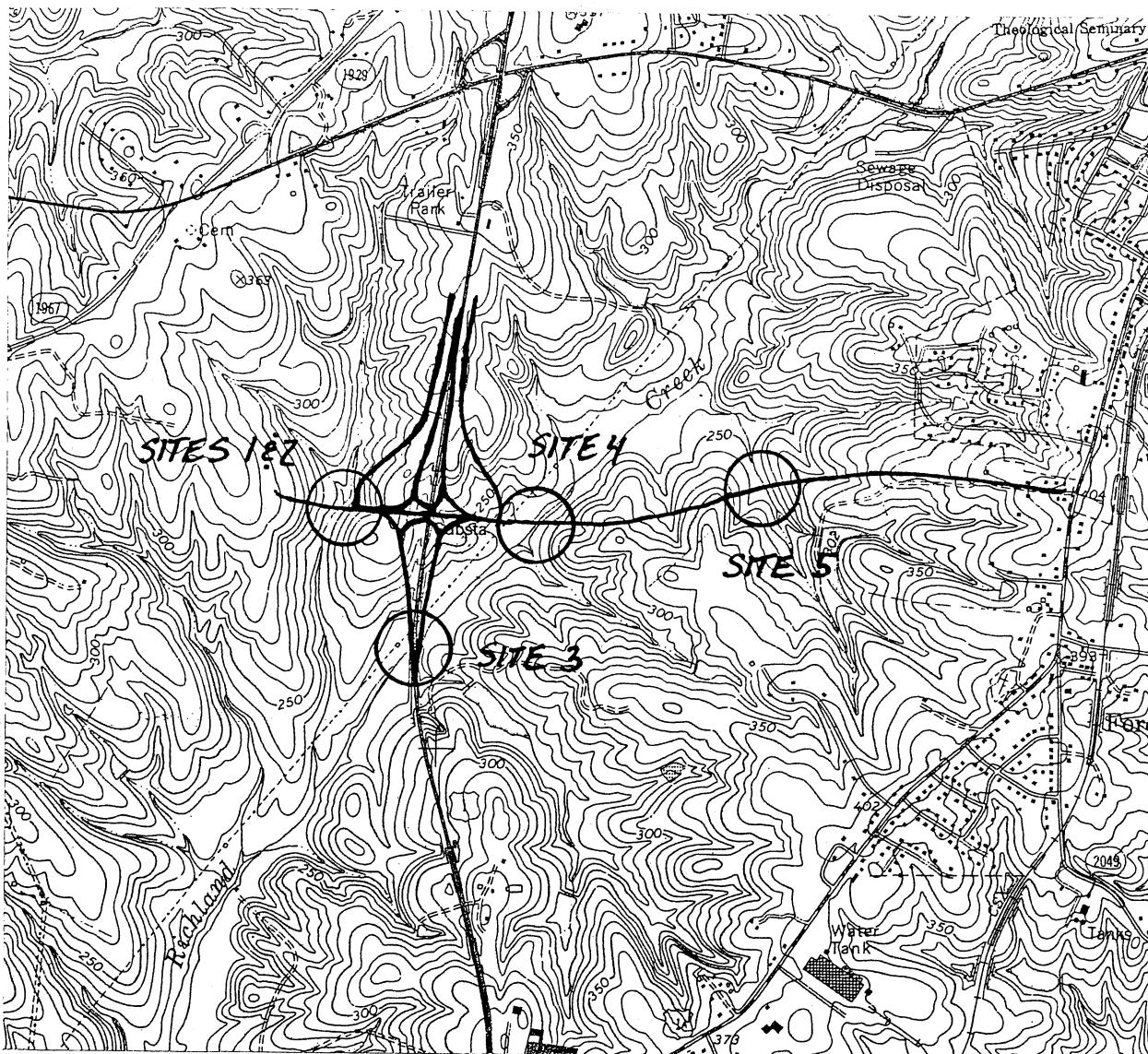
In order to satisfy regulatory assurances that mitigation will be performed; the NCDWQ requires a formal letter from EEP indicating their willingness and ability to provide the mitigation work requested by NCDOT. The NCDOT requests such a letter of confirmation be addressed to Mr. John Hennessy of NCDWQ, with copies submitted to NCDOT.

If you have any questions or need additional information please call Brett Feulner at 715-1488.

Sincerely,  
  
for Gregory J. Thorpe, Ph.D.,  
Environmental Management Director  
Project Development & Environmental Analysis Branch

cc: Mr. David Franklin, USACE, Wilmington  
Mr. John Dorney, Division of Water Quality  
Mr. Travis Wilson, NCWRC  
Mr. Jay Bennett, P.E., Roadway Design  
Mr. Omar Sultan, Programming and TIP  
Ms. Debbie Barbour, P.E., Design Services  
Mr. David Chang, P.E., Hydraulics  
Mr. Greg Perfetti, P.E., Structure Design  
Mr. Mark Staley, Roadside Environmental  
Mr. Terry Gibson, P.E., Division 6 Engineer  
Mr. James Bridges, Project Planning Engineer  
Mr. Jim Rerko, Division 6 Environmental Officer





WETLAND

N.C. DEPT. OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
  
WAKE COUNTY  
  
PROJECT: 8.1402501 (R-2809B)  
NC 98 WAKE FOREST BYPASS  
  
SHEET 2 OF 26

# LEGEND

--- WLB ---- WETLAND BOUNDARY



WETLAND



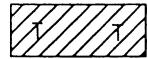
DENOTES FILL IN WETLAND



DENOTES FILL IN SURFACE WATER



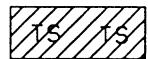
DENOTES FILL IN SURFACE WATER (POND)



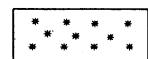
DENOTES TEMPORARY FILL IN WETLAND



DENOTES EXCAVATION IN WETLAND



DENOTES TEMPORARY FILL IN SURFACE WATER



DENOTES MECHANIZED CLEARING

← ← FLOW DIRECTION

TB TOP OF BANK

--- WE --- EDGE OF WATER

--- C --- PROP. LIMIT OF CUT

--- F --- PROP. LIMIT OF FILL

--- ▲ --- PROP. RIGHT OF WAY

--- NG --- NATURAL GROUND

--- PL --- PROPERTY LINE

— TDE — TEMP. DRAINAGE EASEMENT

— PDE — PERMANENT DRAINAGE EASEMENT

— EAB — EXIST. ENDANGERED ANIMAL BOUNDARY

— EPB — EXIST. ENDANGERED PLANT BOUNDARY

— ▽ — WATER SURFACE

X X X LIVE STAKES

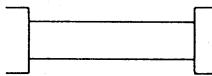


BOULDER

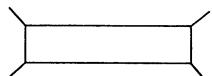
— COIR FIBER ROLLS



ADJACENT PROPERTY OWNER OR PARCEL NUMBER



PROPOSED BRIDGE



PROPOSED BOX CULVERT

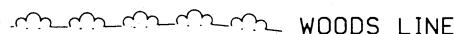


PROPOSED PIPE CULVERT

(DASHED LINES DENOTE EXISTING STRUCTURES)



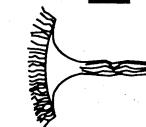
SINGLE TREE



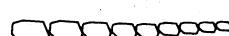
WOODS LINE



DRAINAGE INLET



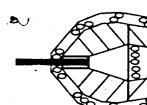
ROOTWAD



VANE



RIP RAP



RIP RAP ENERGY DISSIPATOR BASIN

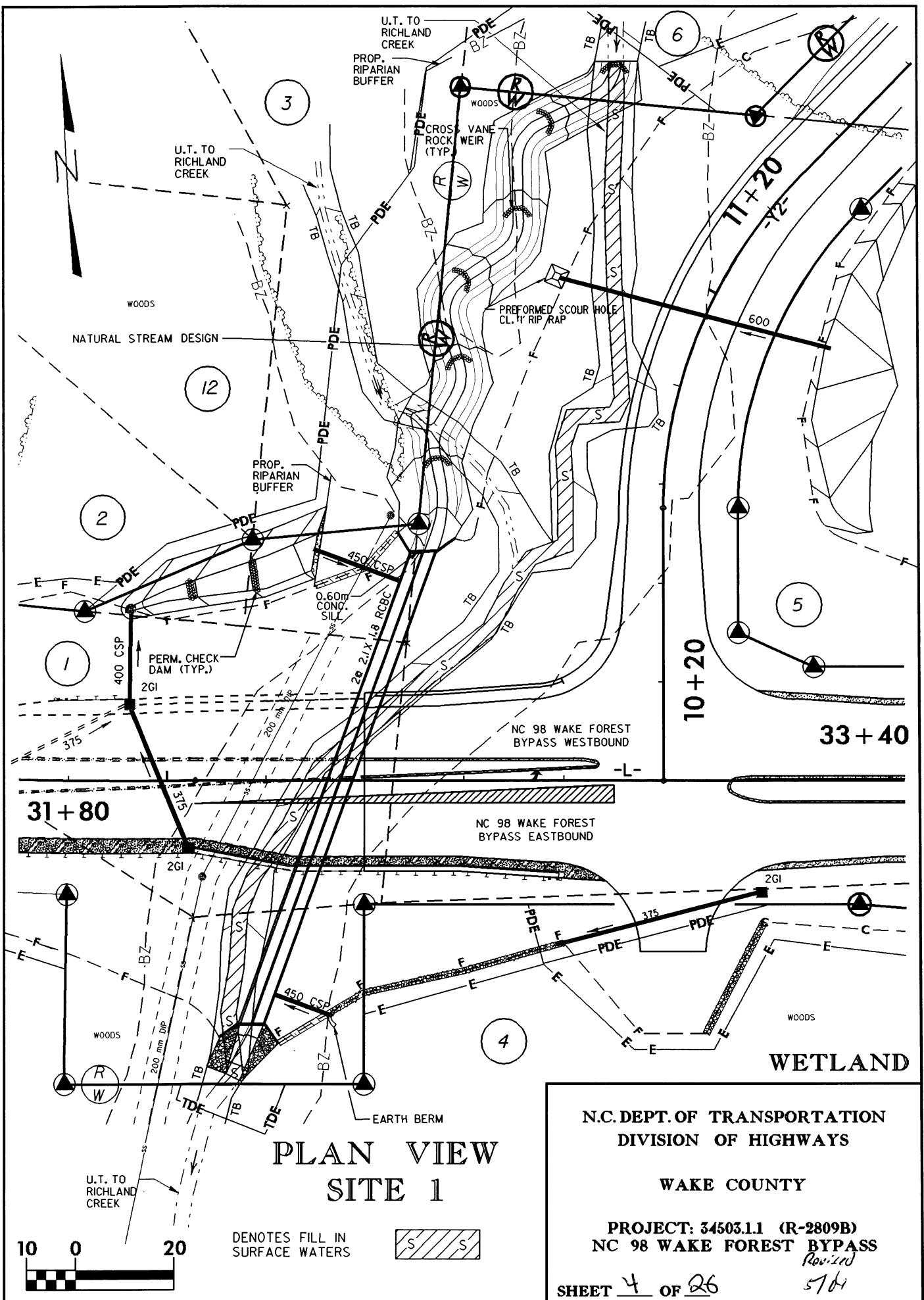
N.C. DEPT. OF TRANSPORTATION  
DIVISION OF HIGHWAYS

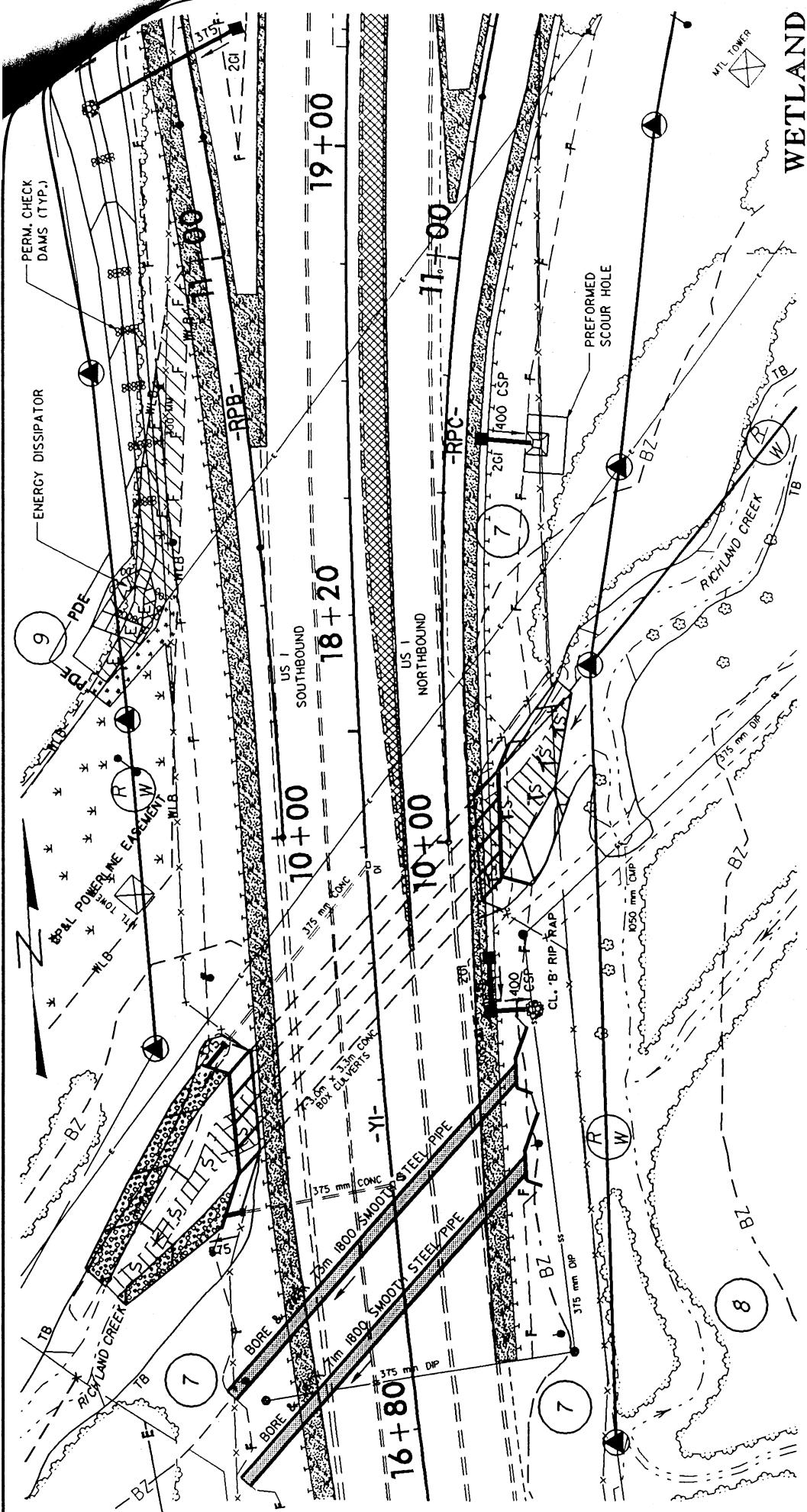
WAKE COUNTY

PROJECT: 8.1402501 (R-2809B)  
NC-98 WAKE FOREST BYPASS

WETLAND

SHEET 3 OF 26





PLAN VIEW  
SITE 3

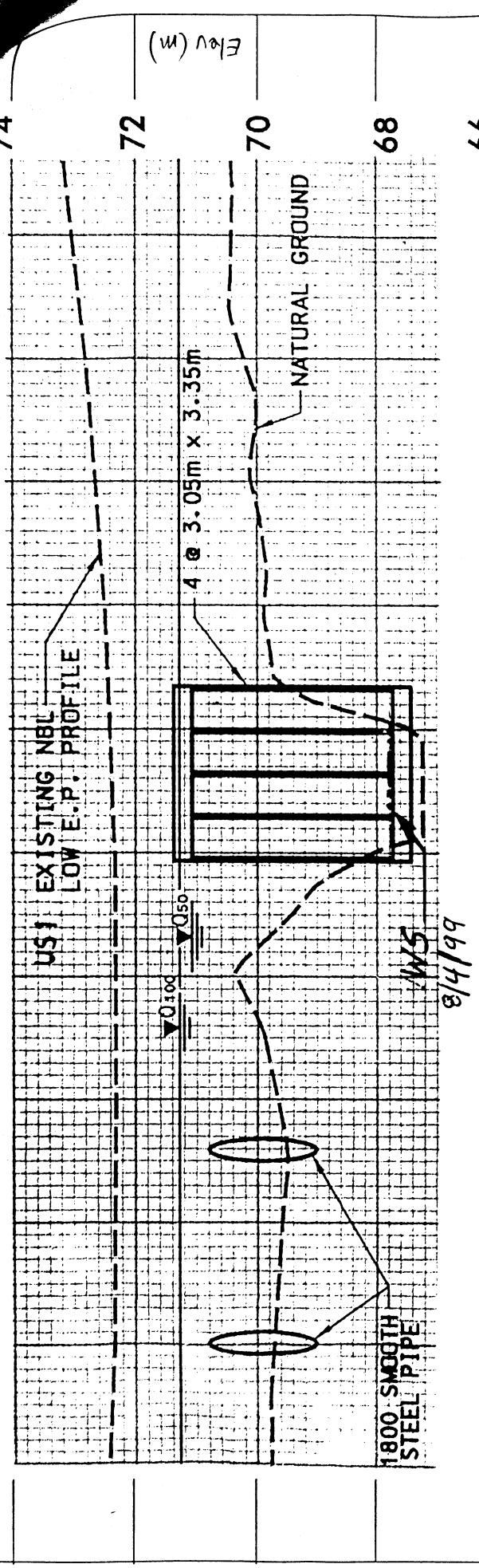
N.C. DEPT. OF TRANSPORTATION  
DIVISION OF HIGHWAYS

## WAKE COUNTY

**PROJECT: 34503.1.1 (R-2809B)  
NC 98 WAKE FOREST BYPASS**

SHEET 15 OF 26 Rev. Aug 2004

20  
0  
10



**NCDOT**  
**DIVISION OF HIGHWAYS**

**PROJECT: 8.1402501 (R-2809B)**  
**NC 98 WAKE FOREST BYPASS**

## PROFILE SITE 3

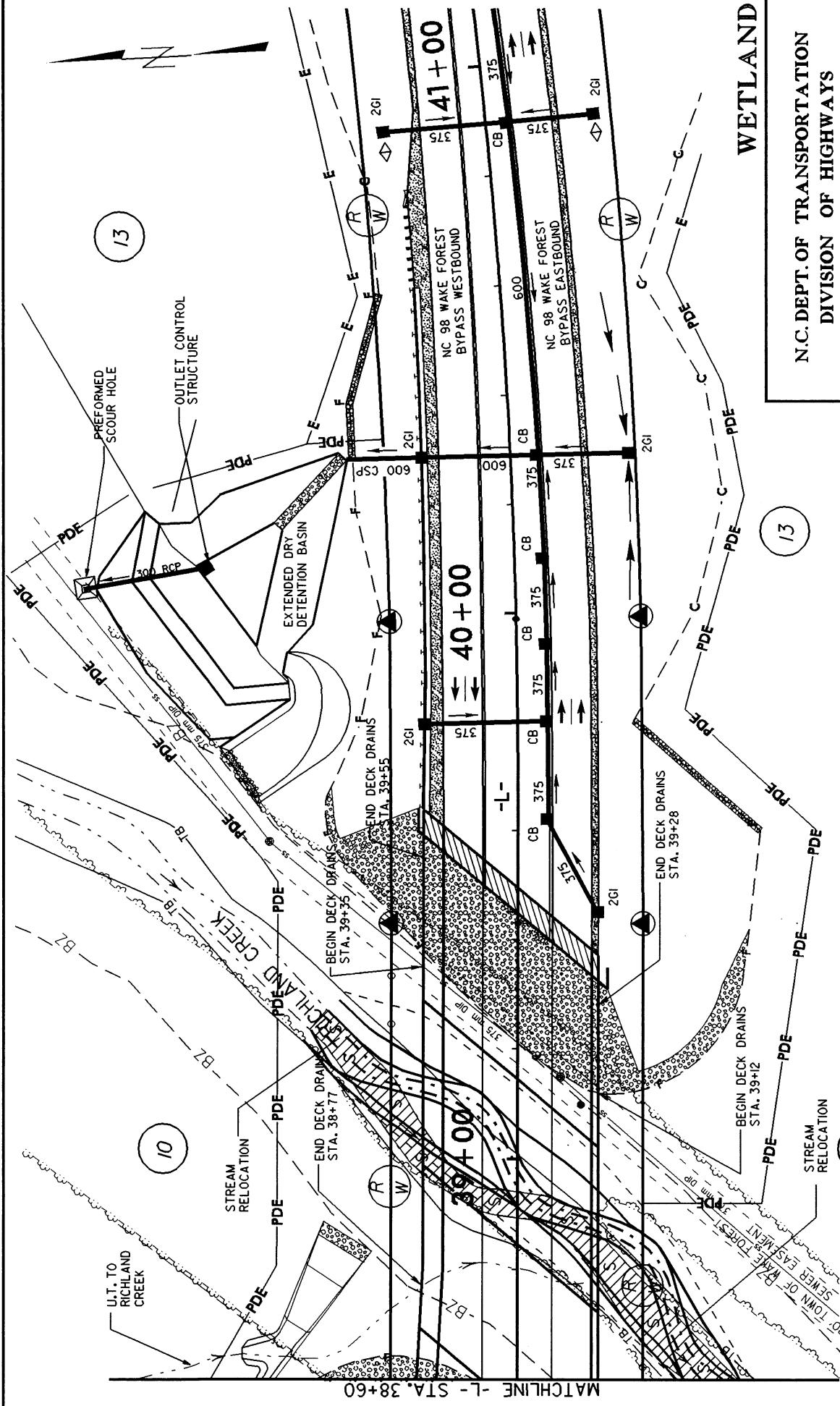
+ 20

8

80

+ 60

40



**PLAN VIEW  
SITE 4**

0 10 20  
[Scale Bar]

DENOTES FILL IN SURFACE WATER

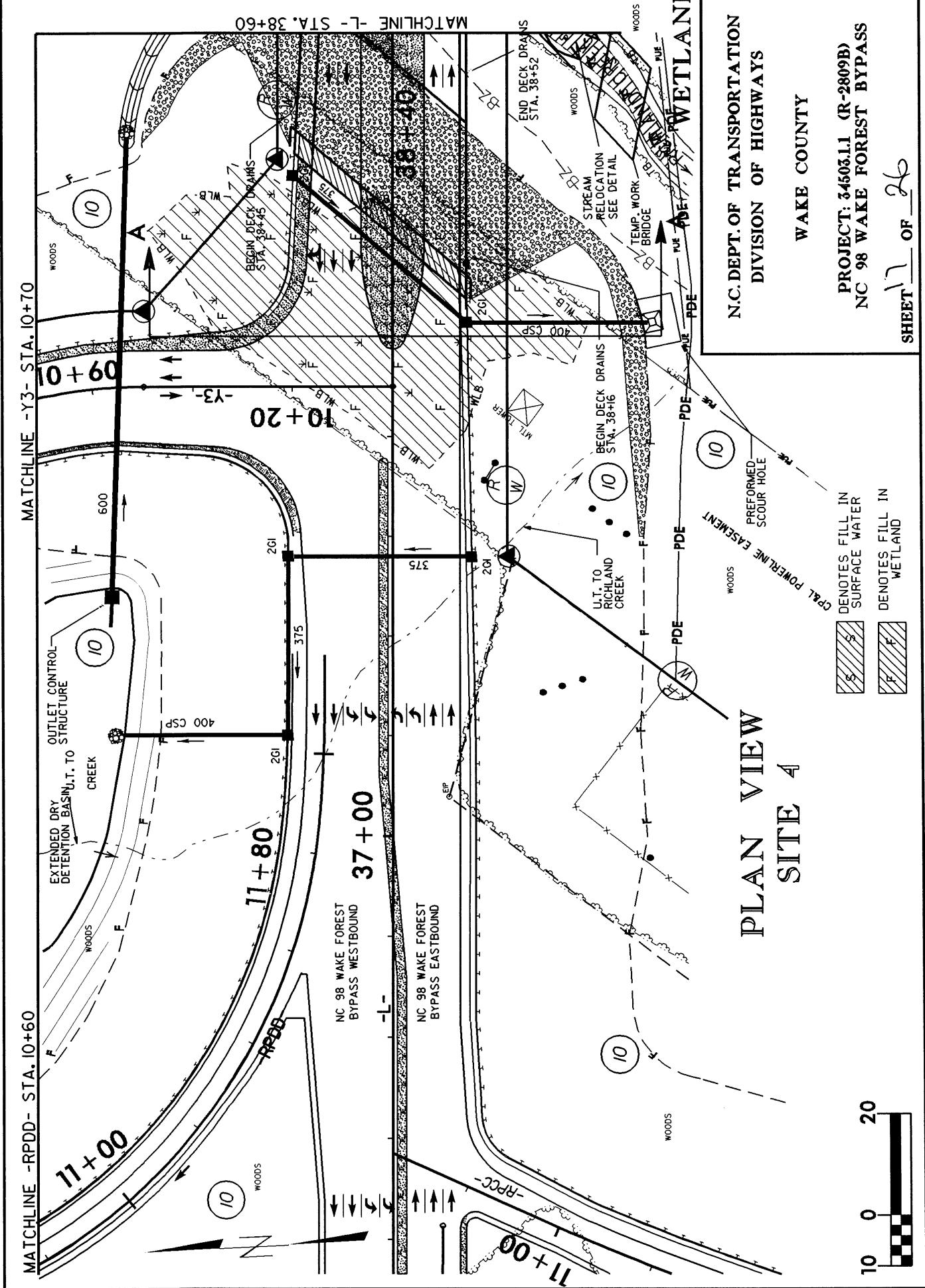
STREAM RELocation

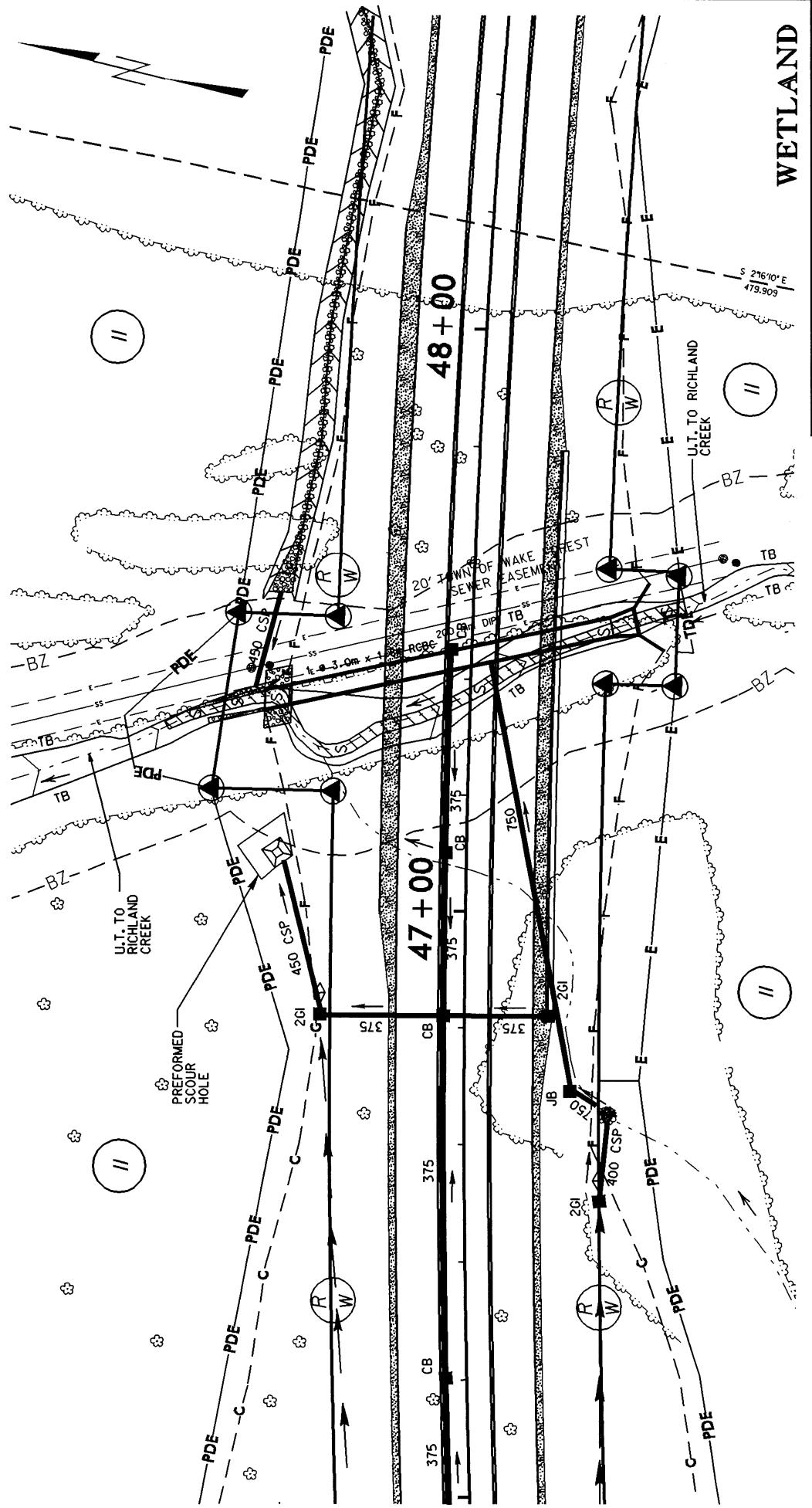
WAKE COUNTY

N.C. DEPT. OF TRANSPORTATION  
DIVISION OF HIGHWAYS

PROJECT: 81402501 (R-2809B)  
NC 98 WAKE FOREST BYPASS

SHEET 18 OF 26





**N.C. DEPT. OF CIVIL ENGINEERING  
DIVISION OF HIGHWAYS**

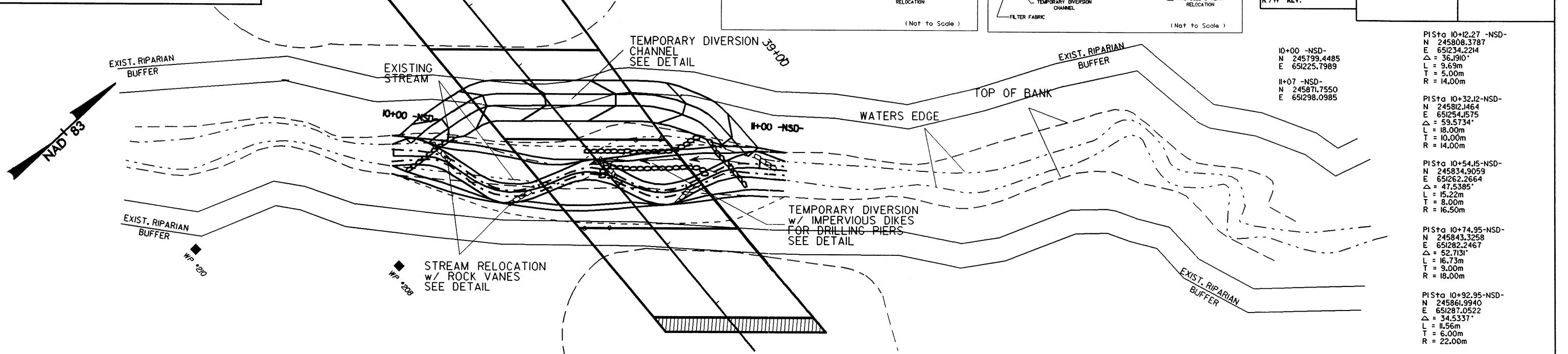
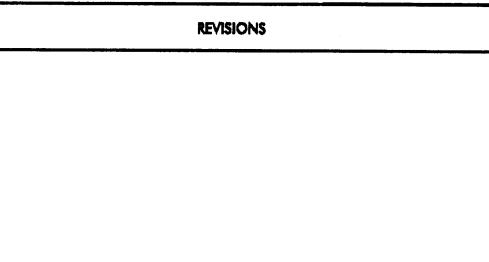
## WAKE COUNTY

**PROJECT: 81402501 (R-2809B)**  
**NC 98 WAKE FOREST BYPASS**  
*(Revised)*

DENOTES FILL IN  
SURFACE WATERS

## PLAN VIEW SITE 5

REVISIONS



PROJECT REFERENCE NO.		SHEET NO.
R-2809B		
R/W SHEET NO.		
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER	
Stream Supplement		
CONST.REV.		10F13
R/W REV.		

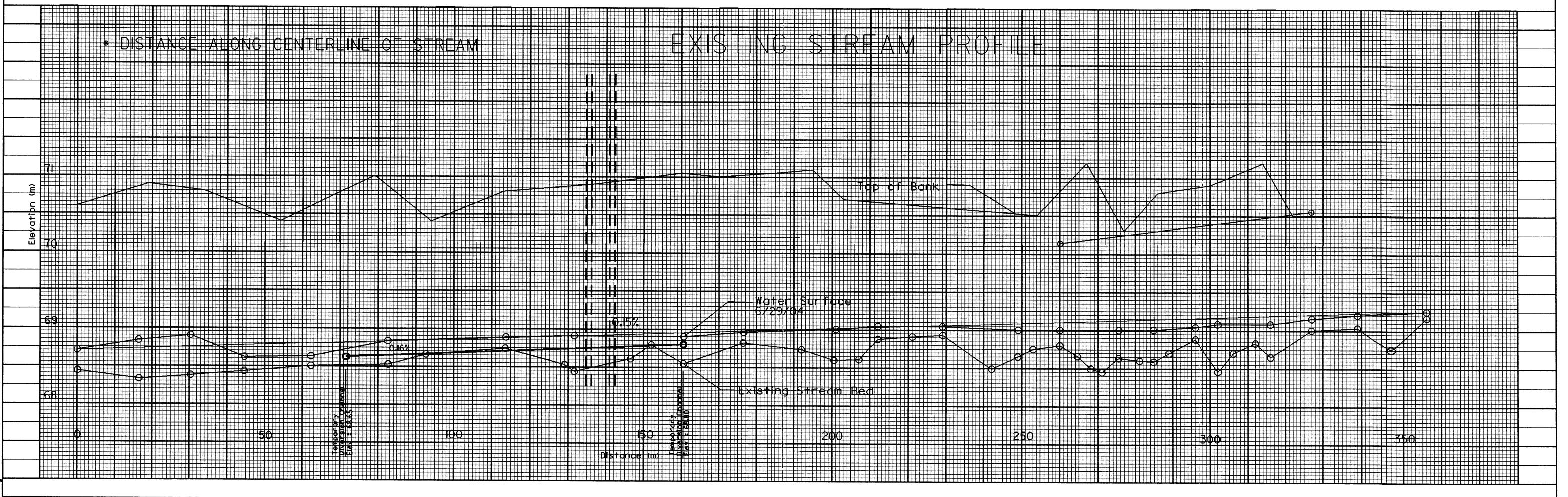
P1 Sta 10+12.27 -NSD-  
N 245808.3787  
E 651234.2214  
 $\Delta$  = 36.191°  
L = 9.69m  
T = 5.00m  
R = 14.00m

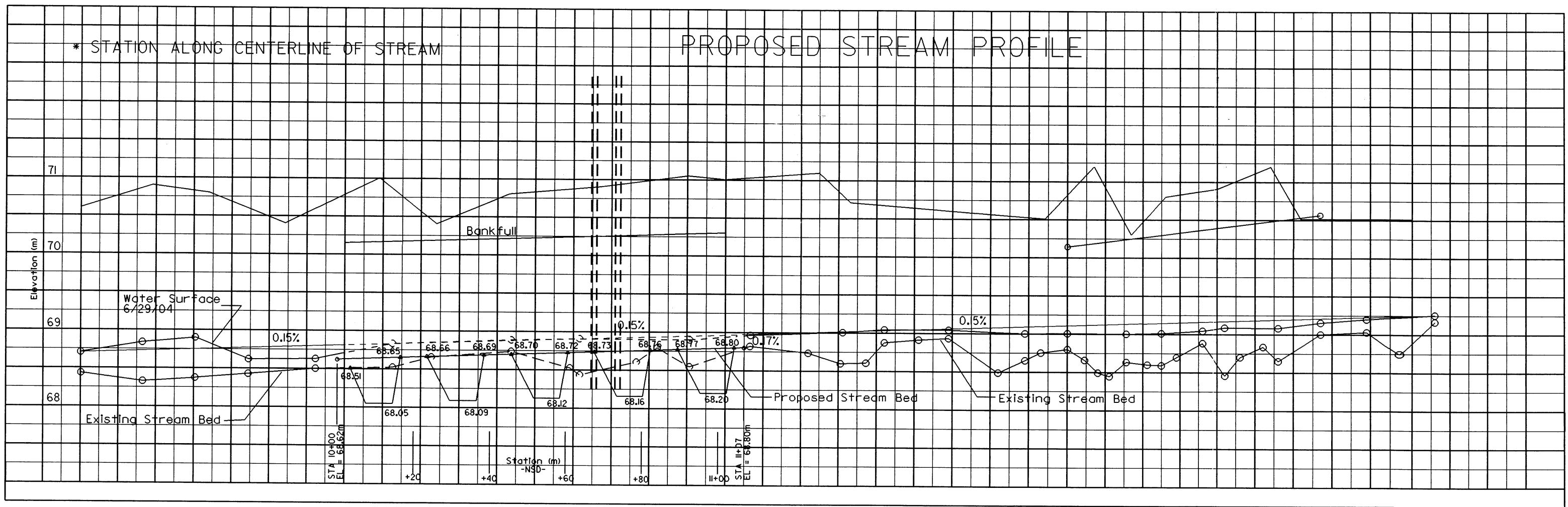
P1 Sta 10+32.12-NSD-  
N 245812.1464  
E 651254.1575  
 $\Delta$  = 59.5734°  
L = 18.00m  
T = 10.00m  
R = 14.00m

P1 Sta 10+54.15-NSD-  
N 245834.3059  
E 651262.2664  
 $\Delta$  = 47.5385°  
L = 15.22m  
T = 8.00m  
R = 16.50m

P1 Sta 10+74.95-NSD-  
N 245843.3258  
E 651282.2467  
 $\Delta$  = 52.7131°  
L = 16.73m  
T = 9.00m  
R = 18.00m

P1 Sta 10+92.95-NSD-  
N 245861.9940  
E 651287.0522  
 $\Delta$  = 34.5337°  
L = 11.56m  
T = 6.00m  
R = 22.00m





\* X-SECTIONS SHOWN PERPENDICULAR TO BANKFULL CHANNEL

74

72

70

68

74

72

70

68

74

72

70

68

74

72

70

68

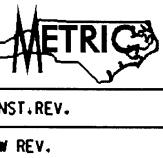
TEMPORARY DIVERSION

25 20 15 10 5 0 5 10 15

Piers

Typical Riffle  
Sta 10+20

Piers



PROJECT REFERENCE NO. R-2809B  
SHEET NO.  
ROADWAY DESIGN ENGINEER HYDRAULICS ENGINEER  
CONST.REV. R/W REV.  
Stream Suppression 1  
3 of 13

TEMPORARY DIVERSION

25 20 15 10 5 0 5 10 15

Piers

Typical Pool  
Sta 10+55

Piers

TEMPORARY DIVERSION

25 20 15 10 5 0 5 10 15

Piers

Typical Riffle  
Sta 10+63

Piers

TEMPORARY DIVERSION

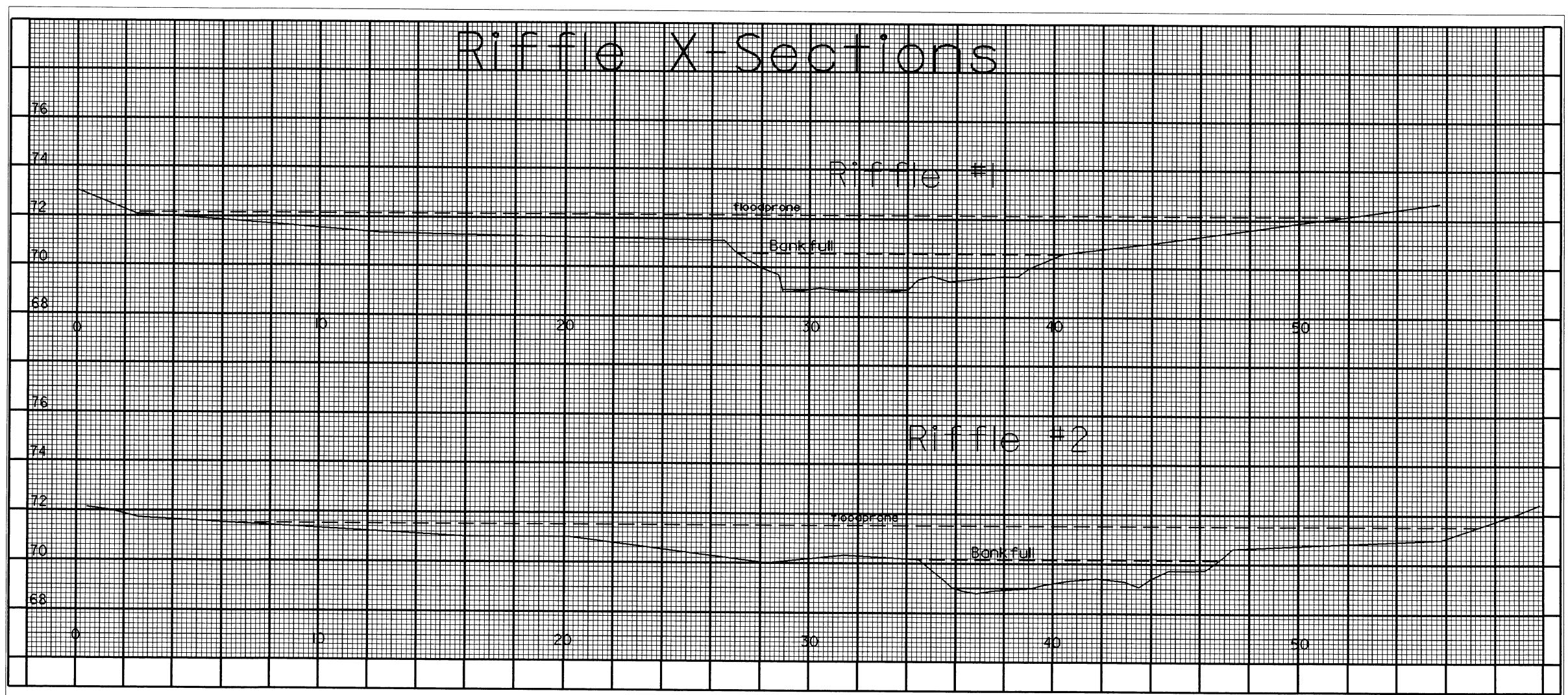
25 20 15 10 5 0 5 10 15

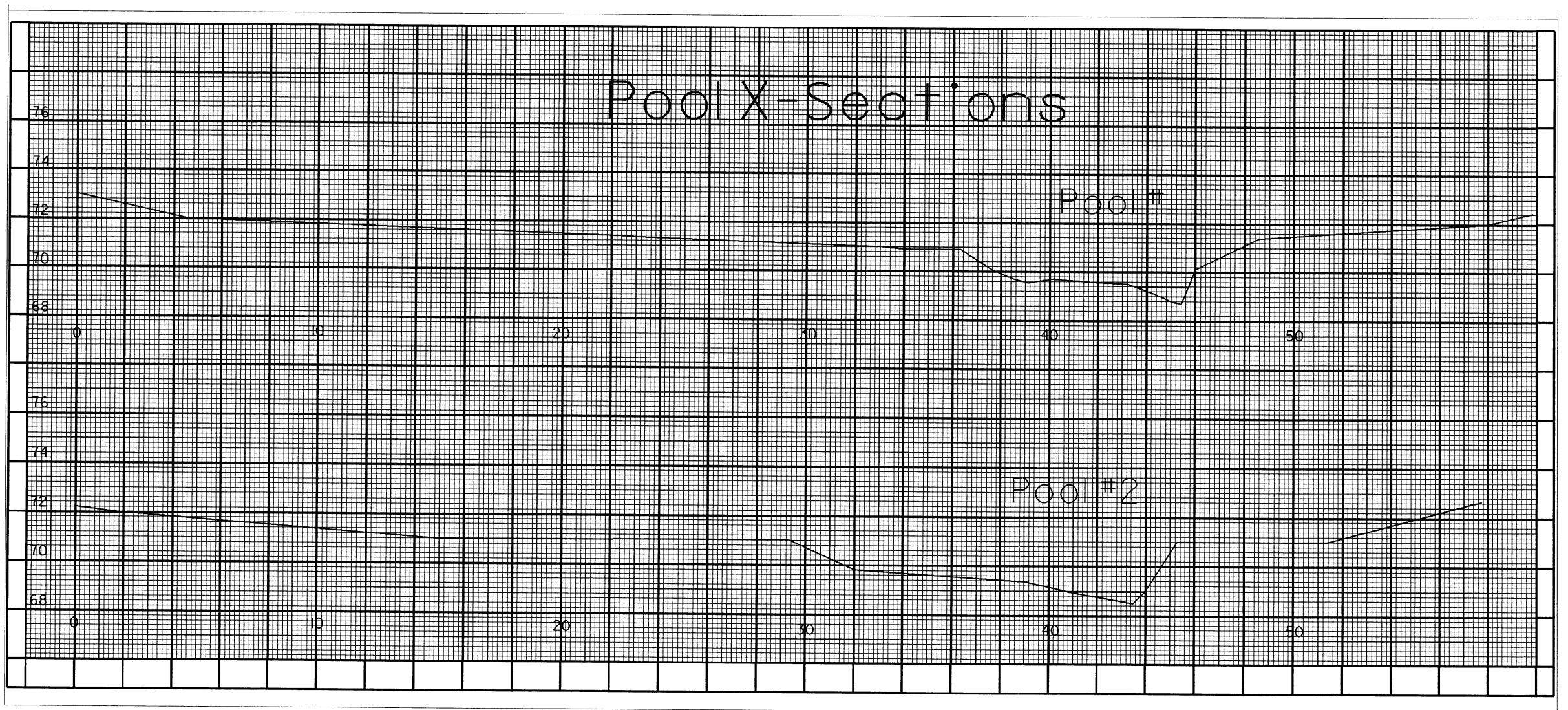
Piers

Temporary Diversion Channel  
at Approx. Sta 10+63

Impervious Dikes

Piers

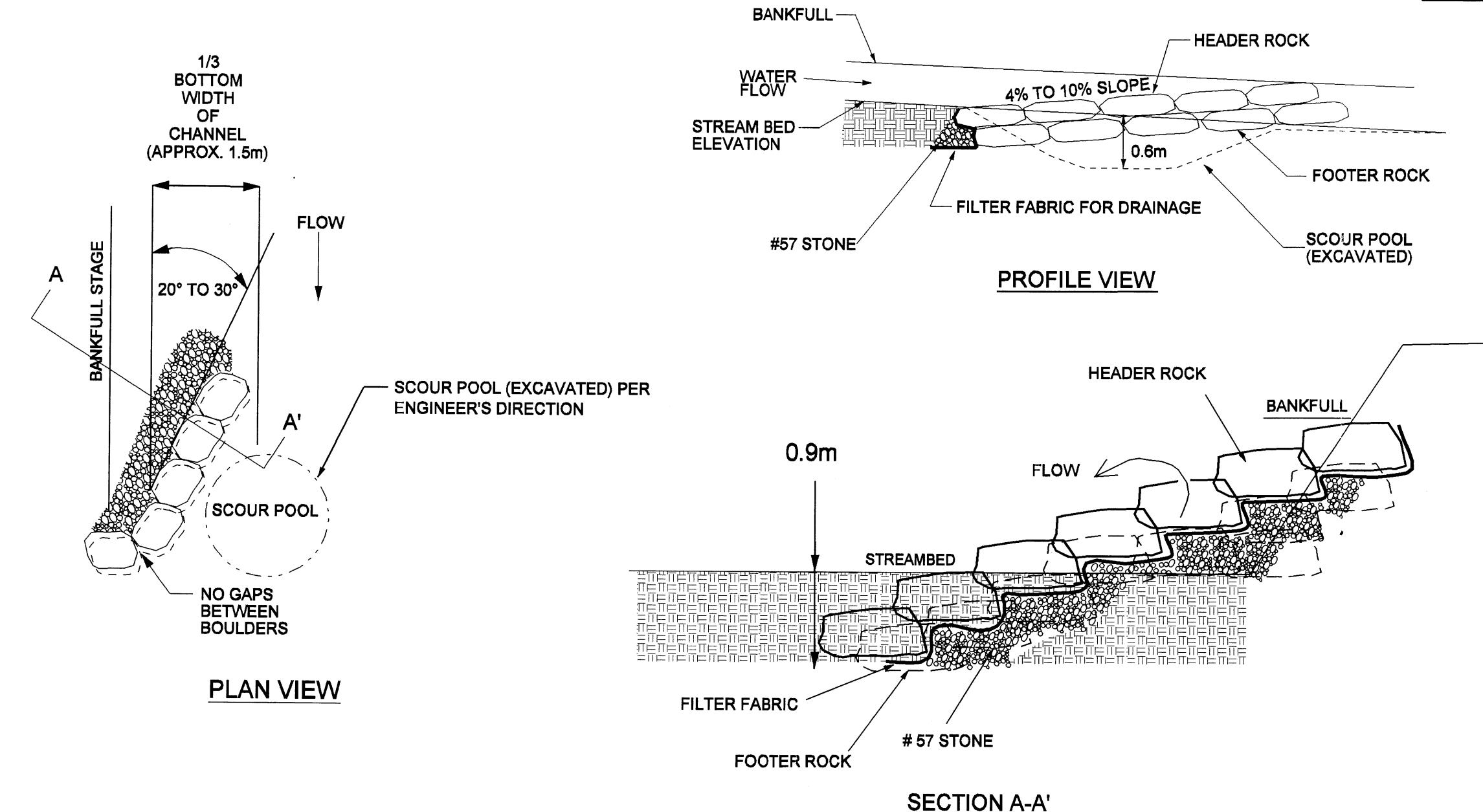




65097

REVISIONS	

PROJECT REFERENCE NO.	SHEET NO.
R-2809B	
R/W SHEET NO.	
ROADWAY DESIGN ENGINEER	HYDRAULICS ENGINEER
CONST.REV.	GOF 13
R/W REV.	



## Rock Vane

SCALE: NTS

HEADER AND FOOTER ROCK SHOULD BE OBLONG AND HAVE MINIMAL DIMENSIONS OF 0.9m x 0.6m x 0.6m

**PROJECT #:** R-2809B  
**COUNTY:** Wake  
**DESCRIPTION:** Stream Relocation at Richland Creek Bridge Crossing  
**STREAM:** Richland Creek

**NATURAL STREAM DESIGN**  
**Sta 39+00 -L-**

A stream relocation design is proposed on the Wake Forest Bypass project. The site is on Richland Creek and is located at the proposed bridge crossing just East of US 1. The design is proposed due to the unforeseen circumstances that 2 of the 7 bridge piers at Bent #2 are located in the stream. Based on original survey data these piers were not shown to be in the stream. However, construction layout and updated topo surveys revealed otherwise.. Presently, it is proposed to relocate the stream to the East away from these piers.

The existing stream was resurveyed to provide updated topo and morphological information. The stream/topo survey included floodplain, top of bank, bankfull, water surface and thalweg data. The "as-built" and "staked" bridge piers were also located. The morphological information included cross sections at riffles, to observe bankfull characteristics, and at pool. A pebble count was also taken at riffle and pool sections.

The basin is suburban and is located in the Blue-Ridge/Piedmont hydrologic region. The crossing is located downstream of the Town of Wake Forest. Basin discharges were computed and prorated using the USGS equations (007-00) and the NC Stream Restoration Institute's Piedmont Regional equations. Data was also analyzed using the HEC-RAS modeling system to compare the accuracy of all the characteristics between the surveyed reference and the regional equations. The basin character (and bankfull morphology) was determined to be suburban. That is, the stream morphology, observed in the field, seemed to fall between those characteristics generated on the NCSRI rural and urban regional curves. The bankfull indicators were close (within 2') to the top of bank to access the floodplain.

The existing stream was observed to change character from the beginning of the survey down through the project and to the end of the survey reach. The upper portion had more sinuosity, better bankfull indicators and more vegetated banks. The downstream portion had little to no sinuosity, poor bankfull indicators, trapezoidal channel dimension and unstable/unvegetated banks, especially at bends. Most of the floodplain has minimal vegetation due to recent utility clearing. The stream was observed to have a meandering thalweg within the main channel banks. While the main stream channel is slightly meandering the thalweg has more significant meandering. The stream was observed to have a significant sediment supply and deposition. Based on the observed field data, NCSRI regional information and hydraulic modeling the existing stream was classified as a C4/E4 stream.

The proposed stream was designed to improve conveyance of the bankfull discharge. These improvements propose to maintain the bankfull area while at the same time flattening side slopes, improving the low flow channel conveyance, providing improved sinuosity and excavating the high banks in certain areas so the floodplain can be accessed more efficiently. A meandering thalweg is also proposed within the main stream channel. To aid in bank stability, rock vanes are proposed in the bend/pool areas. Also, coir fiber mat will be placed on the banks. This will assist in stabilizing the banks and thus assist in establishing vegetation along the stream banks. The stream profile will be at or near that of the existing stream. With the modifications to the stream pattern and dimension it is believed an improved C4/E4 stream will be provided.

The bed material was found to be fine gravel in the riffles and coarse sand in the pools. Shear stress, sediment transport and stream power properties for fine gravel were analyzed. Shear stresses were calculated based on velocities and flow depths generated from the HEC-RAS modeling system. This information was then compared to values for critical velocity and shear stress for fine gravel in the HEC-15 and HDS-5 manuals from the FHA. The Shields Diagram was also used to observe the size of particle moved by the stream energy. The comparison showed the proposed stream to be within acceptable velocity and shear stress limits that would allow proper sediment transport under bankfull conditions.

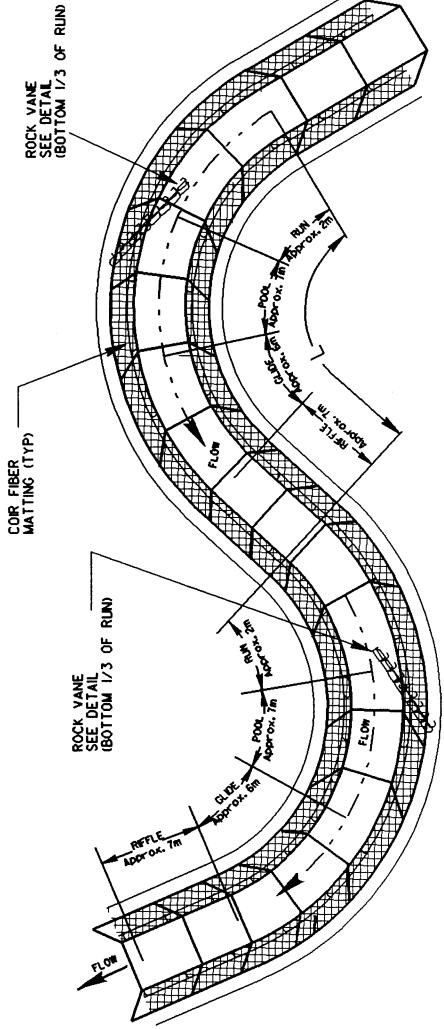
## Appendix B

## Morphological Measurement Table

Variables	Existing Channel	Proposed Reach	USGS Station	** Reference Reach	** Reference Reach
1. Stream type	C4/E4	C4/E4	N/A	N. Potts Crd (Rural E)	McMullen Crk (Urban E)
2. Drainage area	9.72 mi <sup>2</sup> (25.2 km <sup>2</sup> )	9.72 mi <sup>2</sup> (25.2 km <sup>2</sup> )		9.6 mi <sup>2</sup> (24.9 km <sup>2</sup> )	7.0 mi <sup>2</sup> (18 km <sup>2</sup> )
3. Bankfull width	13.1m (43ft)	15.2m (50ft)		8m (25.4ft)	14m (47ft)
4. Bankfull mean depth	1.06m (3.5ft)	0.91m (3.0ft)		1.1m (3.5ft)	1.5m (4.5ft)
5. Width/depth ratio	12.4	16.7		7.3	9.3
6. Bankfull cross-sectional area	13.9 m <sup>2</sup> (150 ft <sup>2</sup> )	13.9m <sup>2</sup> (150ft <sup>2</sup> )		8.3m <sup>2</sup> (89.6ft <sup>2</sup> )	21.0m <sup>2</sup> (227ft <sup>2</sup> )
7. Bankfull mean velocity	1.6 m/s (5.2 ft/s)	0.9m/s (3.0 ft/s)		1.7m/s (5.5 ft/s)	1.3m/s (4.4 ft/s)
8. Bankfull discharge, cfs	22 cms (780 cfs)	22 cms (780 cfs)		14 cms (507 cfs)	28 cms (990 cfs)
9. Bankfull max depth	1.59m (5.2ft)	1.5m (5.0ft)			
10. Width of floodprone area	47m (154ft)	60m (197ft)			
11. Entrenchment ratio	3.6	4.0			
12. Meander length	28m-45m	39m			
13. Ratio of meander length to bankfull width	2.1-3.4	2.6			
14. Radius of curvature	7.3m-29m	14m-22m			
15. Ratio of radius of curvature to bankfull width	0.6-2.2	1.2			
16. Belt width	12m-22m	18m			
17. Meander width ratio	1.2	1.3			
18. Sinuosity (stream length/valley length)	1.09	1.09			
19. Valley slope	0.11%	0.11%			
20. Average slope	0.15%	0.17%		0.12%	0.40%
21. Pool slope	0.00%	0.00%			
22. Ratio of pool slope to average slope	0.00	0.00			
23. Maximum pool depth	1.8m (6.0ft)	2.1m (7.0ft)			
24. Ratio of pool depth to average bankfull depth	1.70	2.3			
25. Pool width	13.3m (44ft)	15.2m (50ft)			
26. Ratio of pool width to bankfull width	1.01	1.00			
27. Pool to pool spacing	20m-30m	22m (72ft)			
28. Ratio of pool to pool spacing to bankfull width	1.5-2.3	1.5			
29. Ratio of lowest bank height to bankfull height (or max bankfull depth)	0.57	0.66			

# STREAM DETAIL

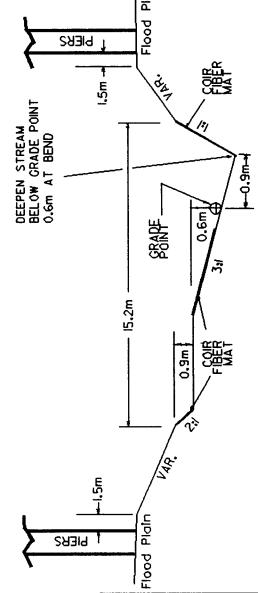
L = LENGTH ALONG STREAM CENTERLINE



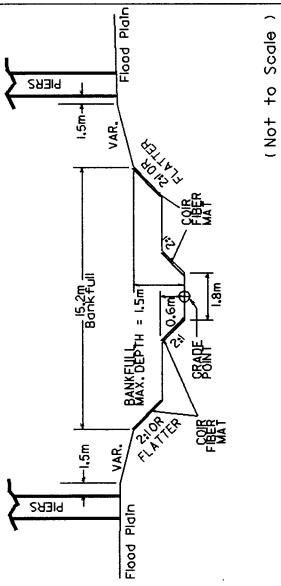
## NOTES:

PLANTINGS SHOULD BE PLACED ABOVE BANKFULL DEPTH.  
ROCK VANES TO BE PLACED IN BOTTOM ONE THIRD OF RUN  
ROCK SHOULD BE OBLONG IN SHAPE AND HAVE MINIMUM DIMENSIONS OF 0.9m x 0.6m x 0.6m (SEE ROCK VANE DETAIL)

CHANNEL DETAIL  
PROPOSED TYPICAL POOL SECTION  
@ BEND (MEANDER)



CHANNEL DETAIL  
PROPOSED TYPICAL RIFFLE SECTION



NATURAL CHANNEL DESIGN TYPICALS

**NC DOT**  
**DIVISION OF HIGHWAYS**  
**WAKE COUNTY**  
**PROJECT: 81402501 (R-2809B)**  
**NC 98 WAKE FOREST BYPASS**

SHEET 6 OF 13

THE REFERENCE REACH FIELD BOOK

17

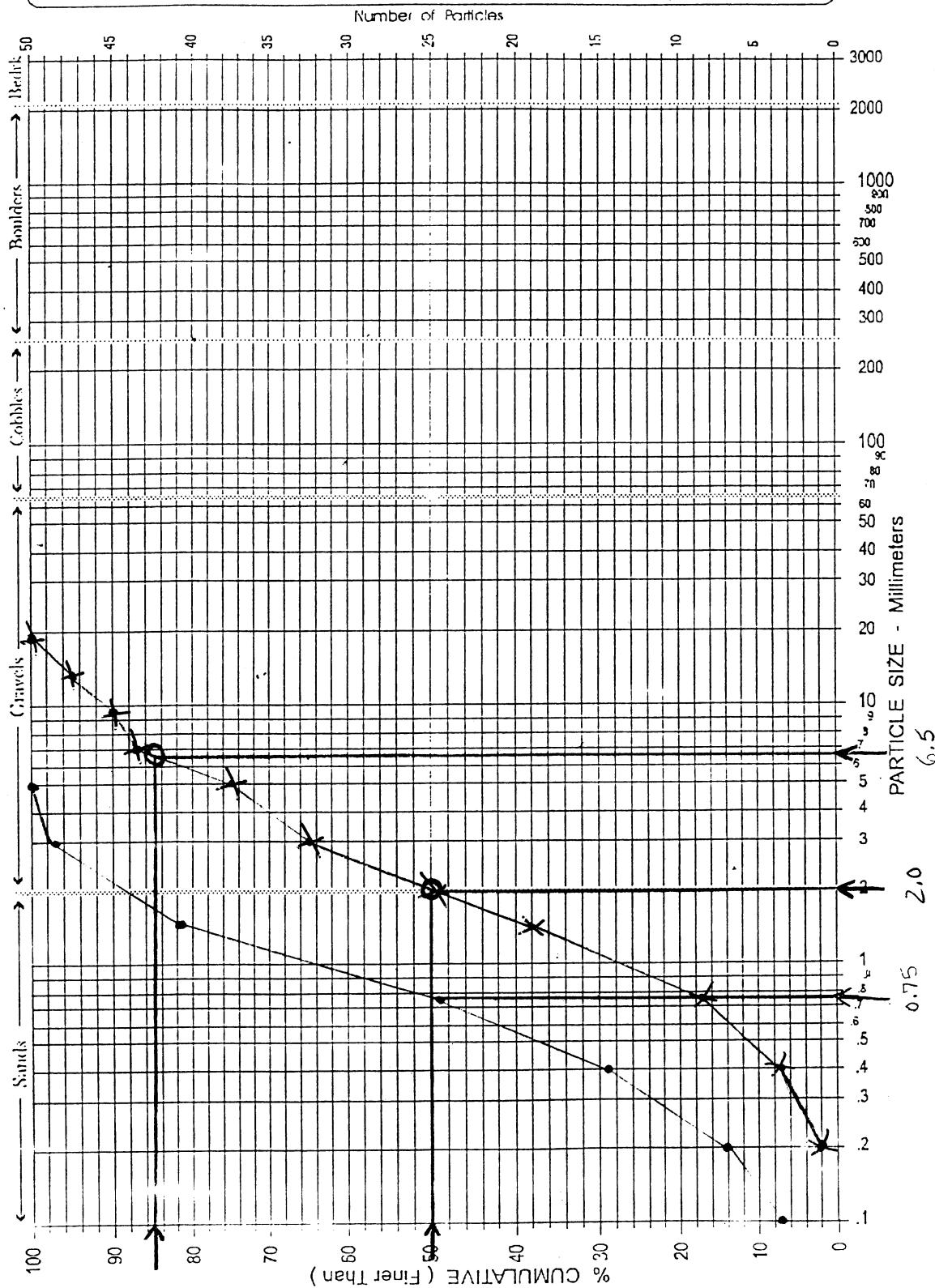
PEBBLE COUNT DATA

GAGE:

No:

Reach:

Date:



Richland Creek

R-2809S

X X Riffle  
— Pool

**Richland Creek Stream Site (R-2809B)**  
**Sta 39+00 -L-**

**SEDIMENT TRANSPORT ANALYSIS**

Station/Description	Flow Depth (ft)	Flow Slope (ft/ft)	Shear Stress (lb/ft <sup>2</sup> )	Bed Material	Velocity (ft/s)
Proposed	3.0	0.0017	0.312	Gravel/Sand	4.7
Existing	3.5	0.0015	0.299	Sand/Silt	5.7

**Note:** Velocities determined from HEC-RAS Model

**Proposed Morphology**

$$\begin{aligned} \text{** Critical Shear Stress} &= \frac{0.23}{\text{lb/ft}^2} \\ \text{*** Permissible Velocity} &= \frac{3.7}{\text{ft/s}} \end{aligned}$$

Fine Gravel w/ Water Carrying Sand and Gravel

**\* Shields:**

Particle Size	15.0	mm
Dimensionless Shear Stress	0.0618	lb/ft <sup>2</sup>
Kinematic Viscosity	0.00001400	ft <sup>2</sup> /s
Mass Density	1.94	slugs/ft <sup>3</sup>
Unit Weight (Particle)	165.0	lb/ft <sup>3</sup>
Unit Weight (Water)	62.4	lb/ft <sup>3</sup>
Reynolds Number	1409.7	
Dimensionless Shear Stress from Shields Diagram	0.060	lb/ft <sup>2</sup>

**References:**

- \* Shields Diagram
- \*\* Hydraulic Engineering (HEC) 15 - Chart 1
- \*\*\* Hydraulic Design Series (HDS) 3 - Table 2

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<u>Proposed</u>	<u>Existing</u>	<u>Stream Power:</u>
Q <sub>BKF</sub>	780.0 ft <sup>3</sup> /s	
W/D	16.7	
Side Slope	2.0	
Mannings n	0.032	
Valley Slope	0.0011 ft/ft	
Sinuosity	1.09	
Valley Slope/Sinuosity	0.0010 ft/ft	0.0010 ft/ft
Velocity	4.7 ft/s	5.7 ft/s
Area	150.0 ft <sup>2</sup>	150.0 ft <sup>2</sup>
W <sub>BKF</sub>	50.0 ft	43.0 ft
Base Width	38.0 ft	33.0 ft
Mean Depth	3.0 ft	3.5 ft
Wetted Perimeter	51.0 ft	47.0 ft
Hydraulic Radius	2.94 ft	3.19 ft
<b>Shear Stress</b>	<b>0.19 lb/ft<sup>2</sup></b>	<b>0.20 lb/ft<sup>2</sup></b>
<b>Particle Moved</b>	<b>13.0 mm</b>	<b>14.0 mm</b>
<b>Existing:</b>	<b>stream power = 0.040 lb/ft/sec</b>	<b>Proposed:</b>
		stream power= 0.029 lb/ft/sec

**WETLAND PERMIT IMPACT SUMMARY**

Site No.	Station (From / To)	Structure Size / Type	WETLAND IMPACTS			SURFACE WATER IMPACTS					
			Fill In Wetlands (ac)	Temp. Fill In Wetlands (ac)	Excavation In Wetlands (ac)	Mechanized Clearing (Method III) (ac)	Fill In SW (Natural) (ac)	Fill In SW (Pond) (ac)	Temp. Fill In SW (ac)	Existing Channel Impacted (ft)	Natural Stream Design (ft)
1	-L- 31+96 / -Y2- 11+38	2 @ 21m x 1.8m RCBC	-	-	-	-	0.19	-	-	797.20	383.80
2	-Y2- 10+42L / -Y2- 10+89L	-	-	-	-	-	0.01	-	-	132.20	-
3	-Y1- 16+88L / -RPB- 11+01L	4 @ 3.2m x 3.2m RCBC	0.06	-	0.05	0.02	0.05	-	-	222.40	-
4	-L- 37+74L / 38+34L	4@98' PSG Bridge	0.66	-	-	-	0.15	-	0.03	351.00	351.00
5	-L- 47+09L / 47+70R	1 @ 3.0m X 1.8m RCBC	-	-	-	-	0.04	-	0.01	240.80	-
TOTALS:			0.72	0.00	0.05	0.02	0.43	0.00	0.04	1743.60	734.80

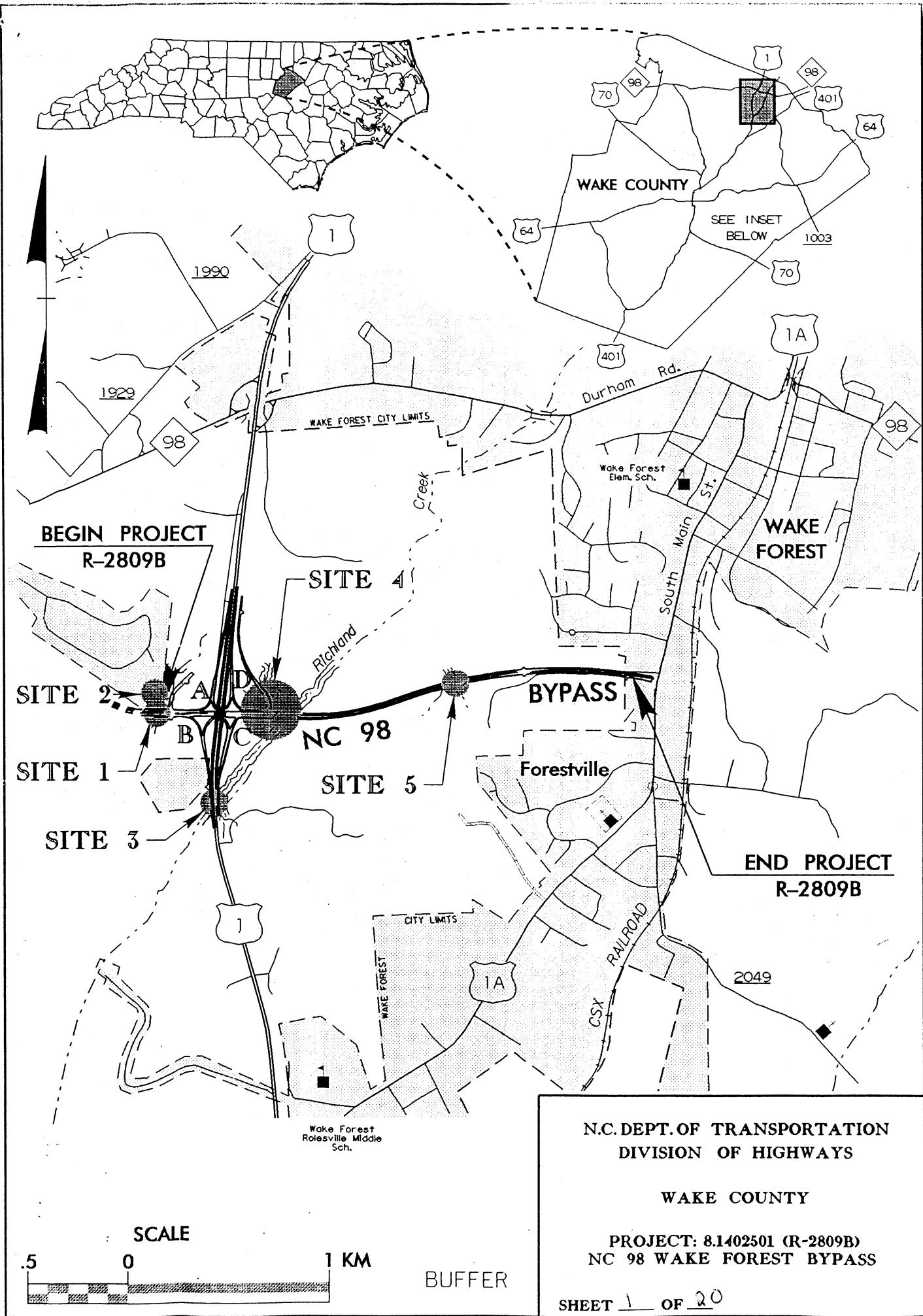
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DIVISION OF HIGHWAYS

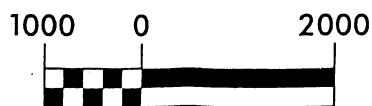
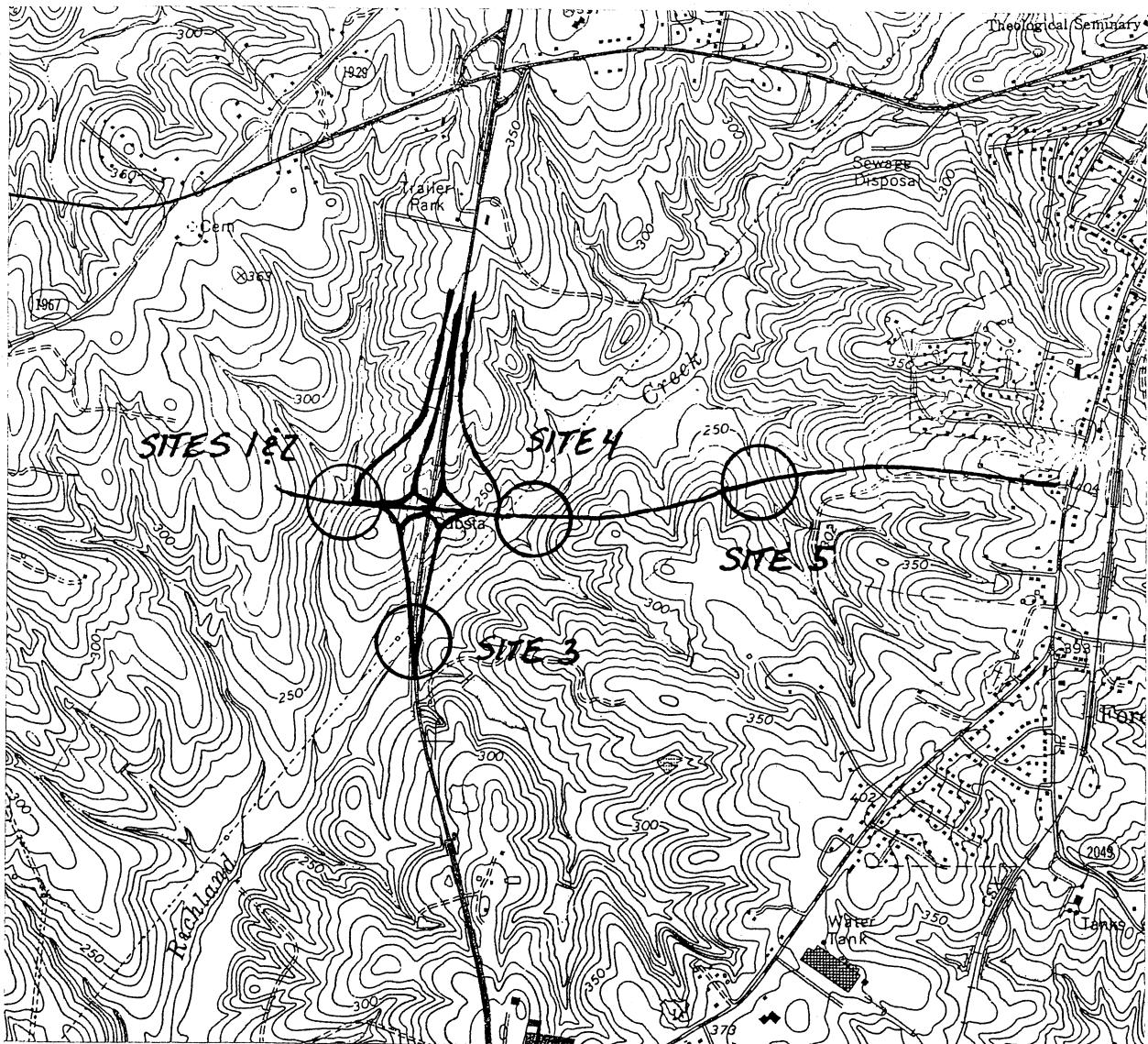
Notes.  
Site 4 temporary stream impacts = 82 feet  
Site 5 temporary stream impacts = 61 feet

WAKE COUNTY

PROJECT 8.1402501 (R-2809B)  
NC 98 WAKE FOREST BYPASS

SHEET  
26 OF 26





BUFFER

N.C. DEPT. OF TRANSPORTATION  
DIVISION OF HIGHWAYS

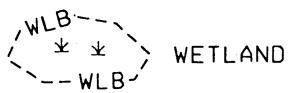
WAKE COUNTY

PROJECT: 8.1402501 (R-2809B)  
NC 98 WAKE FOREST BYPASS

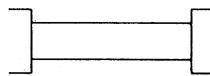
SHEET 2 OF 20

# BUFFER LEGEND

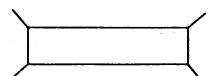
-- WLB --- WETLAND BOUNDARY



WETLAND



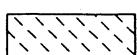
PROPOSED BRIDGE



PROPOSED BOX CULVERT



DENOTES ALLOWABLE IMPACTS ZONE 1



DENOTES ALLOWABLE IMPACTS ZONE 2



DENOTES MITIGABLE IMPACTS ZONE 1



DENOTES MITIGABLE IMPACTS ZONE 2

— BZ — RIPARIAN BUFFER ZONE

— BZ1 — RIPARIAN BUFFER ZONE 1  
30 ft (9.2m)

— BZ2 — RIPARIAN BUFFER ZONE 2  
20 ft (6.1m)

← ← FLOW DIRECTION

— TB — TOP OF BANK

— WE — EDGE OF WATER

— C — PROP. LIMIT OF CUT

— F — PROP. LIMIT OF FILL

— ▲ — PROP. RIGHT OF WAY

— NG — NATURAL GROUND

— PL — PROPERTY LINE

— TDE — TEMP. DRAINAGE EASEMENT

— PDE — PERMANENT DRAINAGE EASEMENT

— EAB — EXIST. ENDANGERED ANIMAL BOUNDARY

— EPB — EXIST. ENDANGERED PLANT BOUNDARY

— ▽ — WATER SURFACE

× × × ×  
× × × ×  
LIVE STAKES

~ ~ BOULDER

— — — CORE FIBER ROLLS

(DASHED LINES DENOTE EXISTING STRUCTURES)

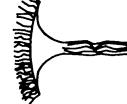
12"-48"  
PIPES  
54" PIPES  
& ABOVE



SINGLE TREE



WOODS LINE



DRAINAGE INLET



ROOTWAD



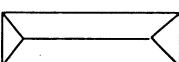
RIP RAP



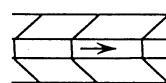
ADJACENT PROPERTY OWNER  
OR PARCEL NUMBER  
IF AVAILABLE



PREFORMED SCOUR HOLE (PSH)



LEVEL SPREADER (LS)



GRASS SWALE

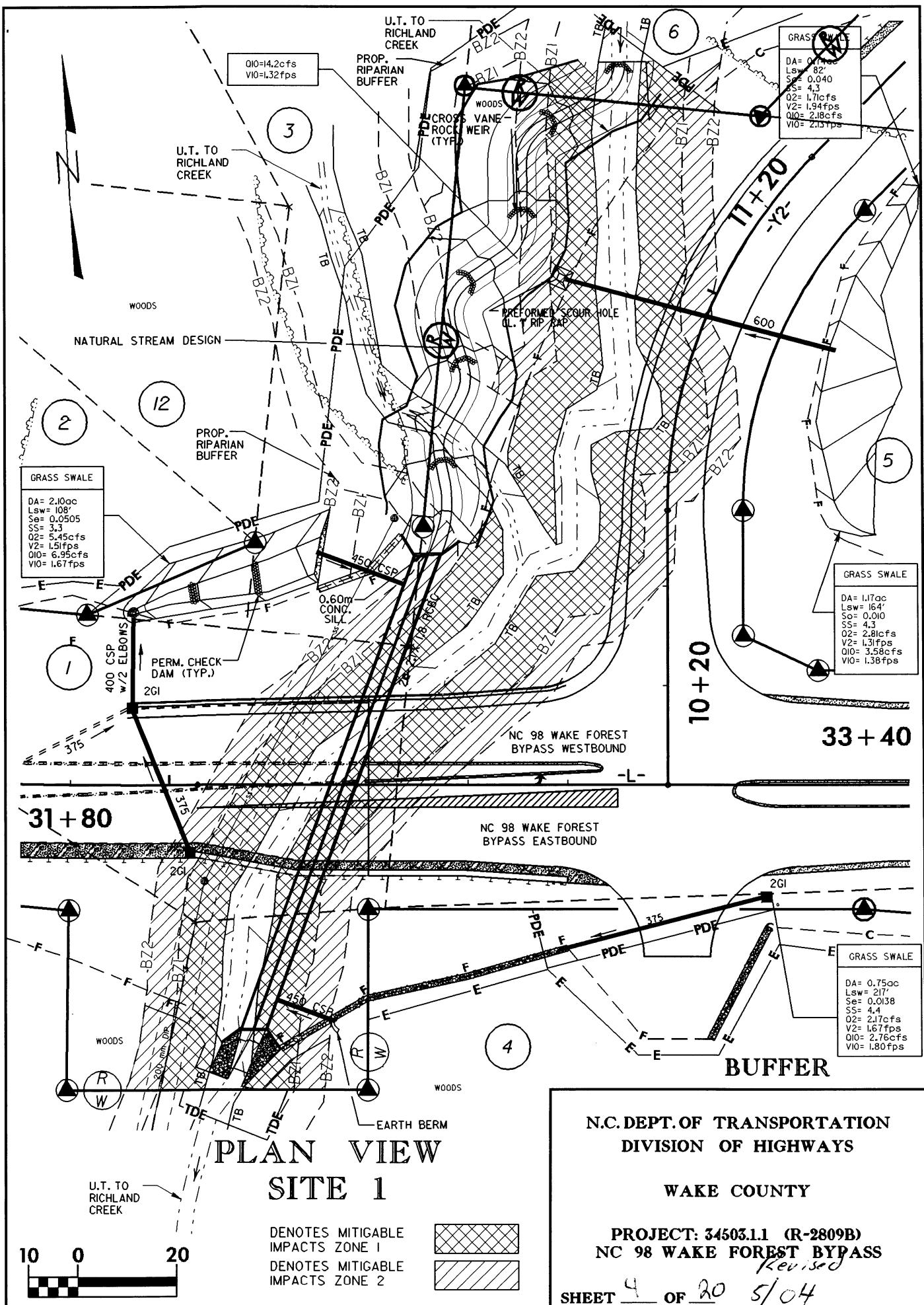
BUFFER

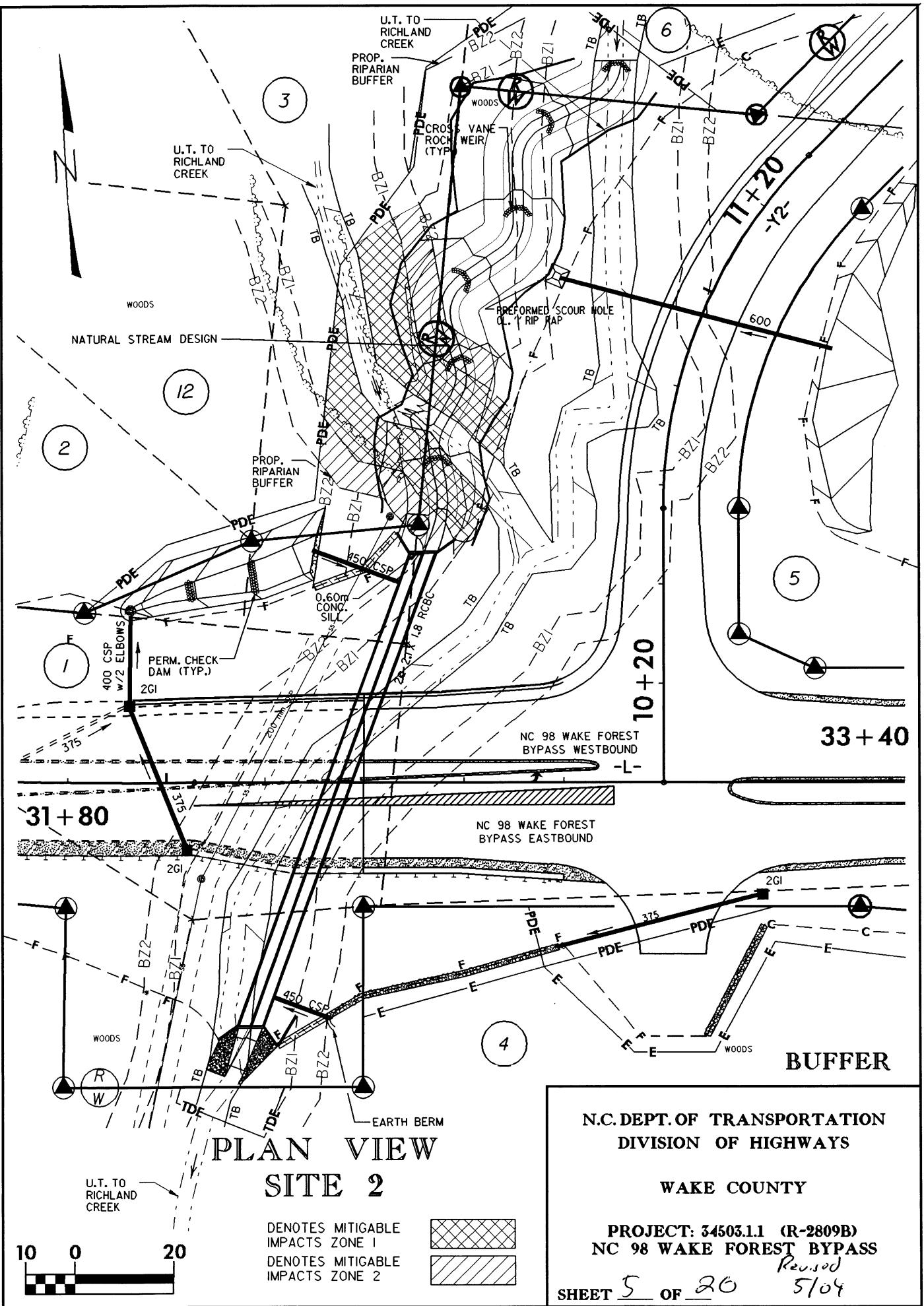
N.C. DEPT. OF TRANSPORTATION  
DIVISION OF HIGHWAYS

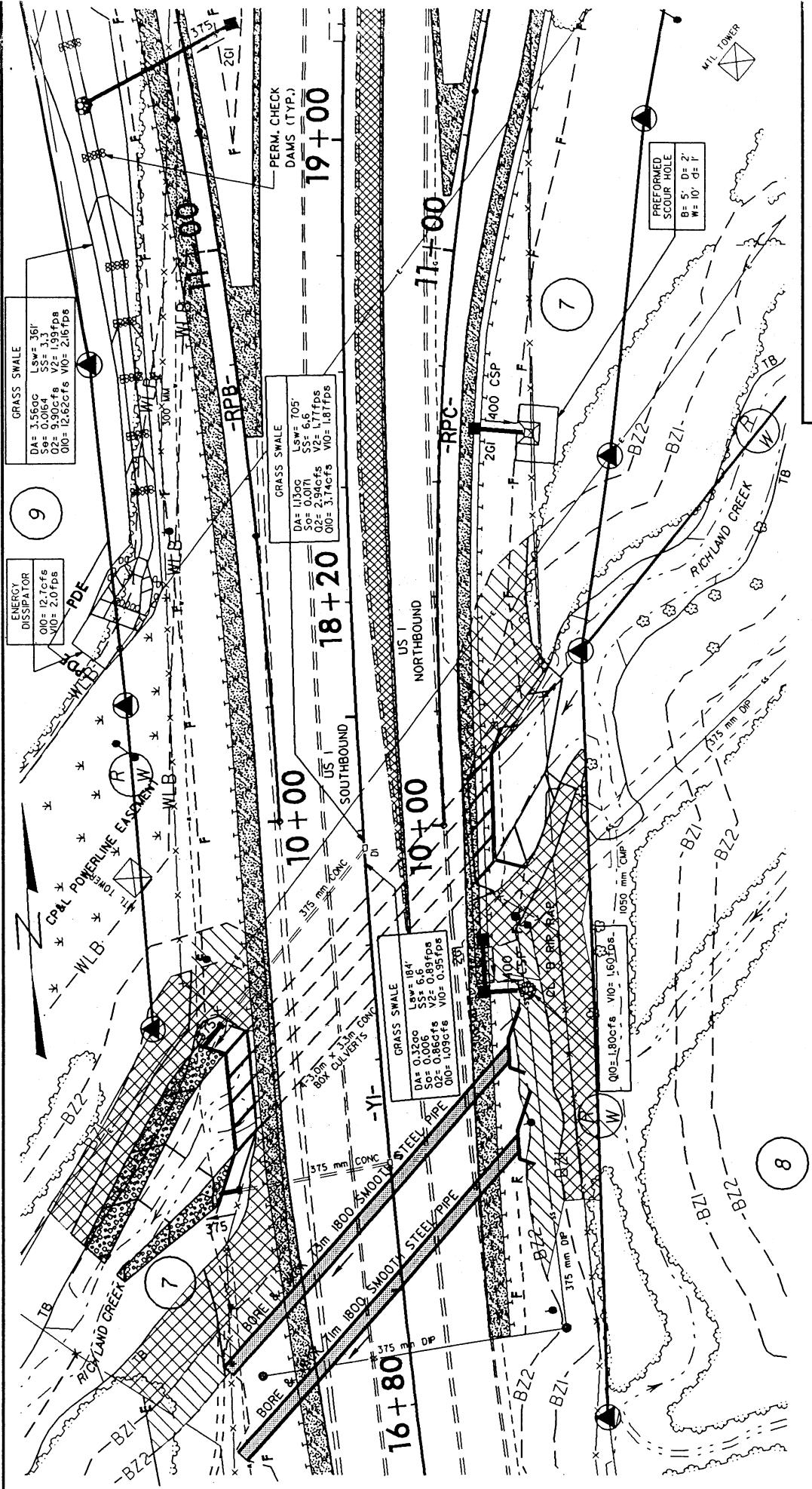
WAKE COUNTY

PROJECT: 8.1402501 (R-2809B)  
NC-98 WAKE FOREST BYPASS

SHEET 3 OF 20







N.C. DEPT. OF TRANSPORTATION  
DIVISION OF HIGHWAYS

WAKE COUNTY

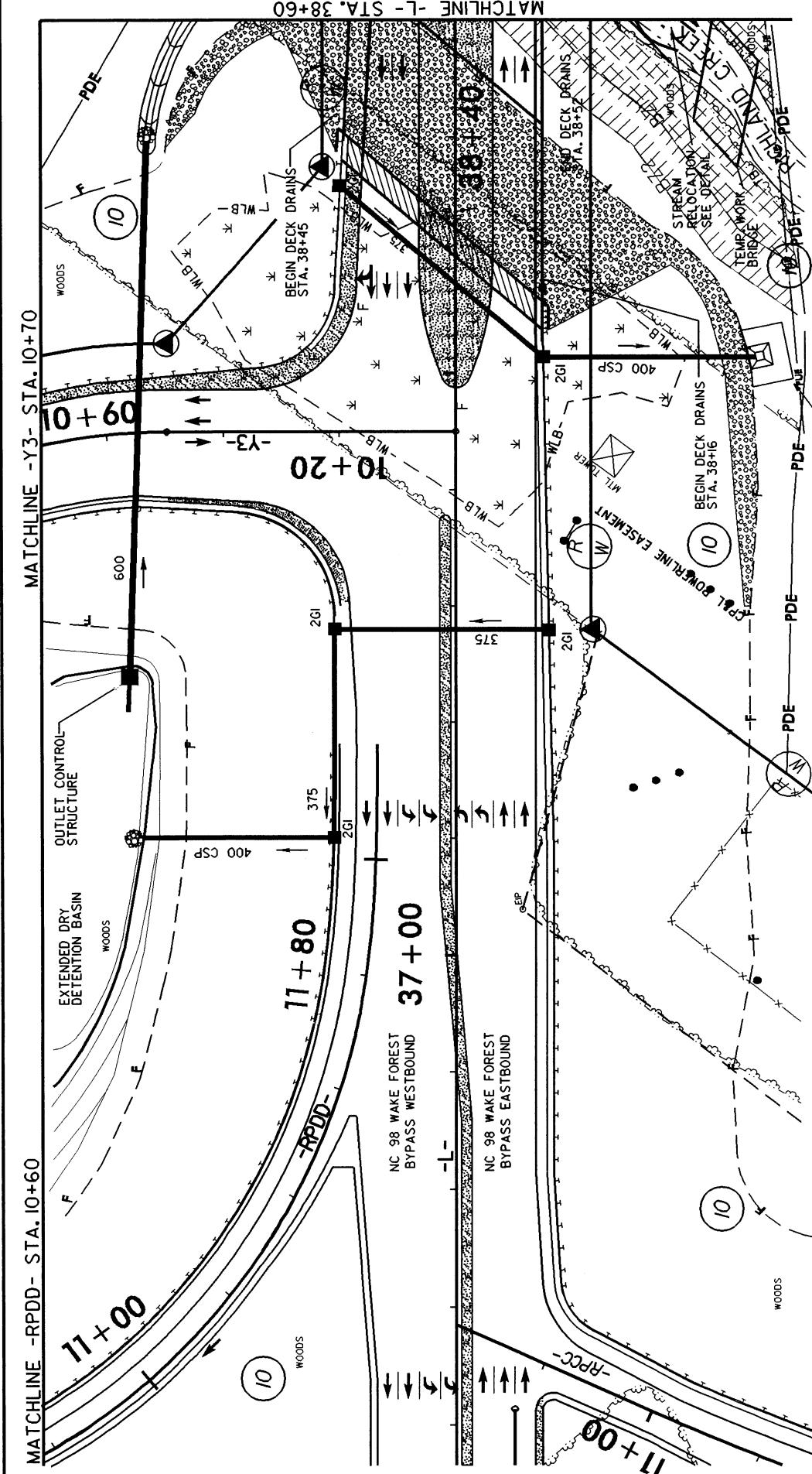
## PLAN VIEW SITE 3

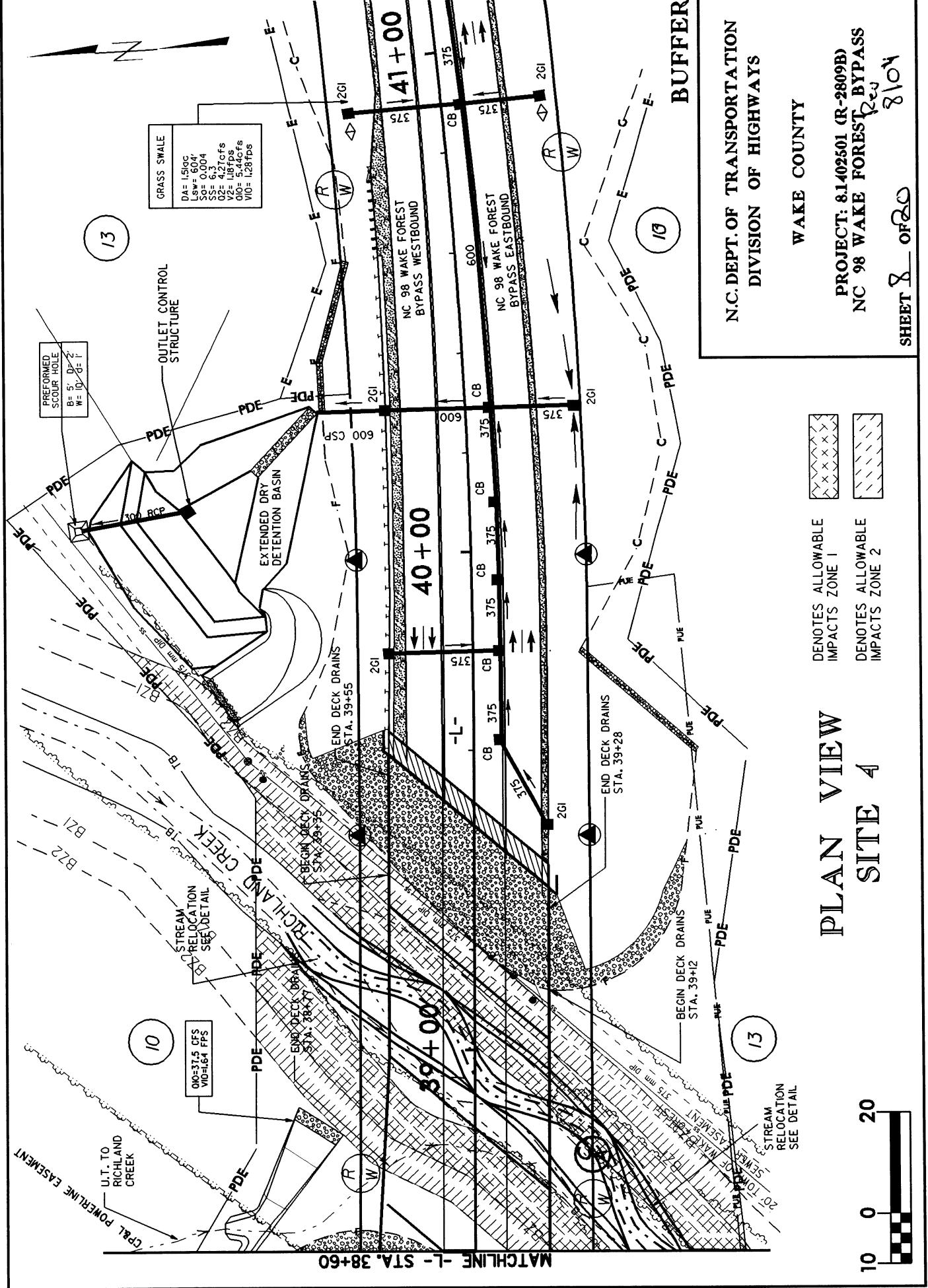
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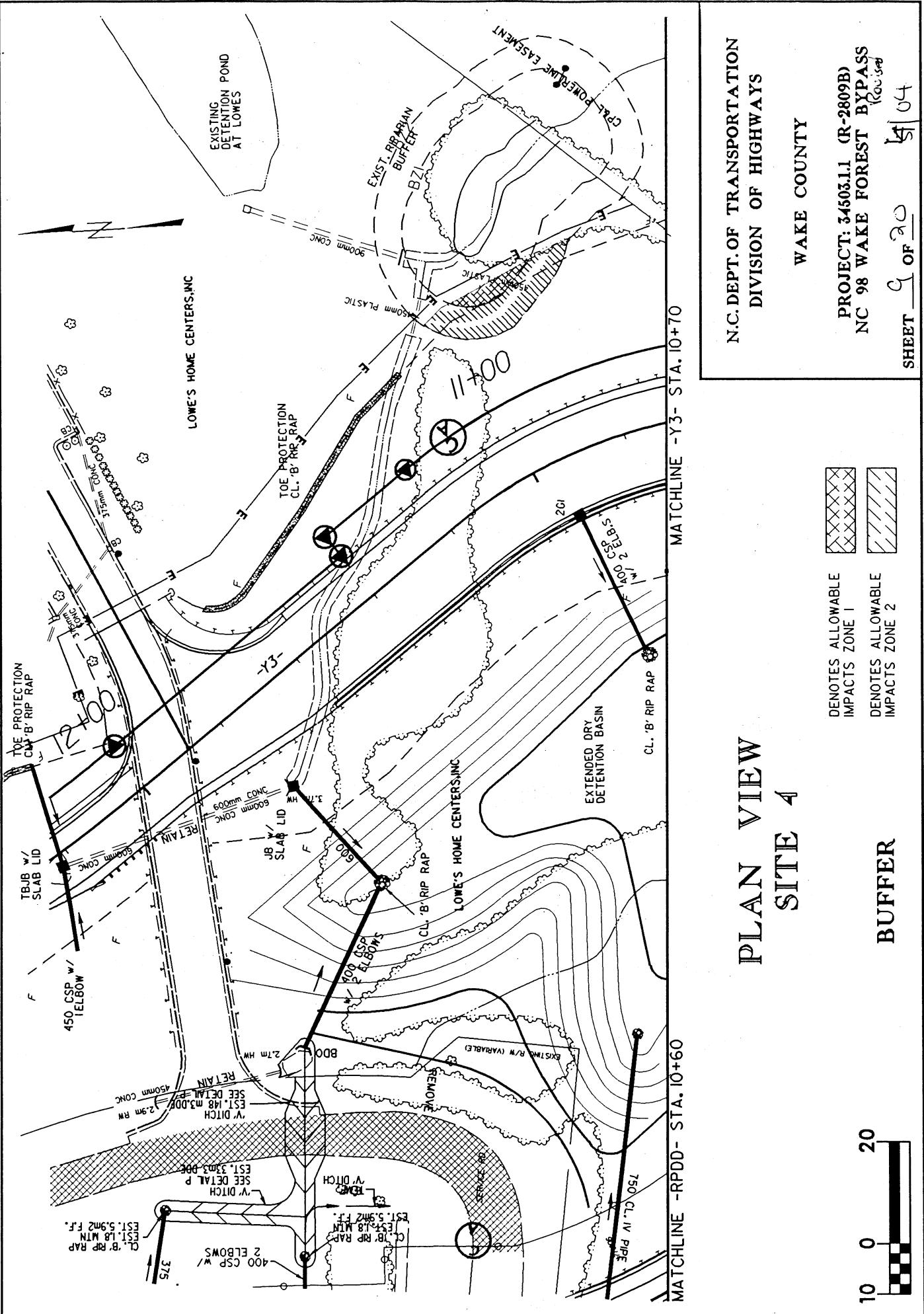


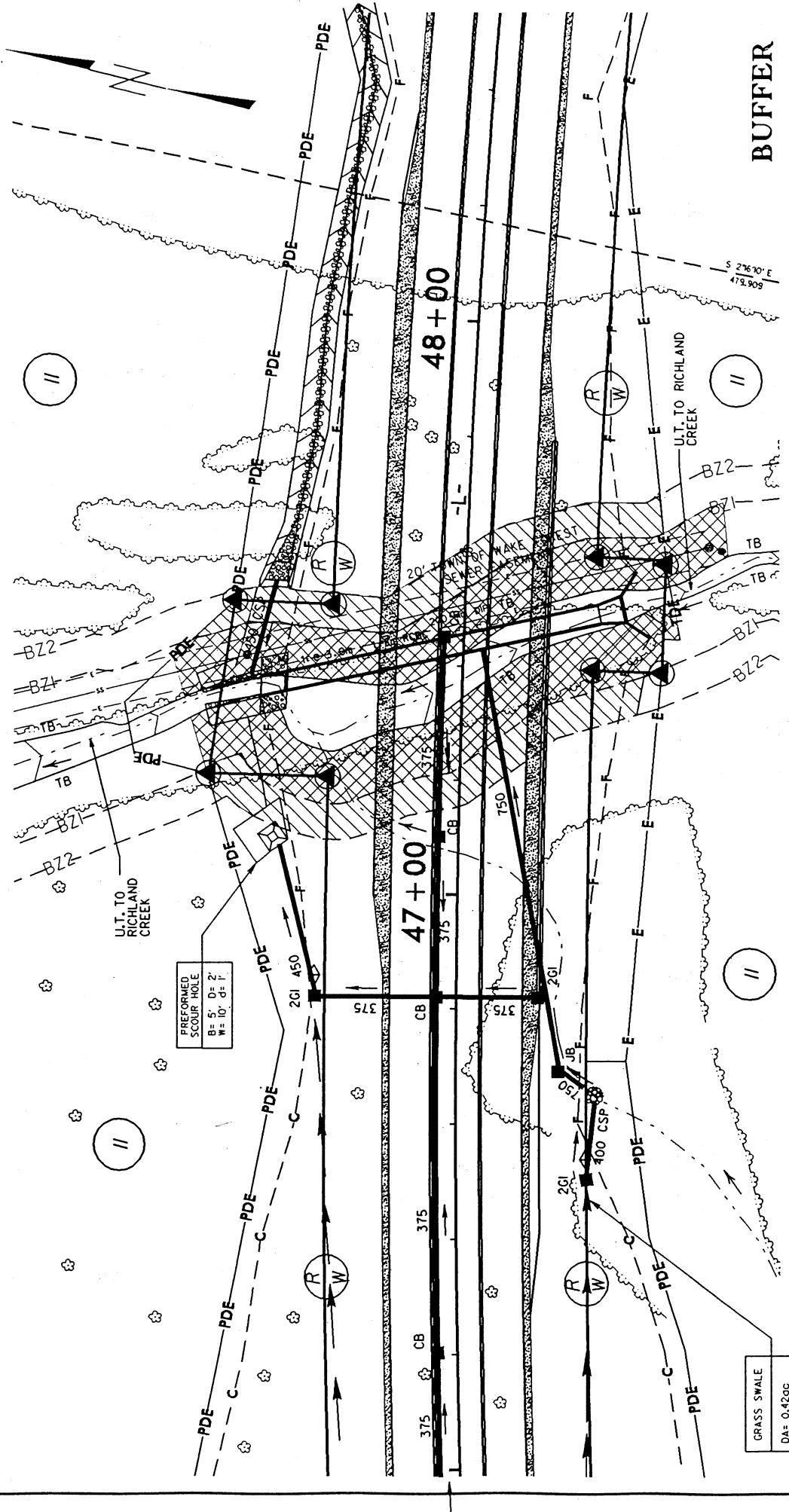
PROJECT: 34503.1.1 (R-2809B)  
NC 98 WAKE FOREST BYPASS

SHEET 6 OF 20





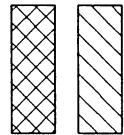




## PLAN VIEW SITE 5

DENOTES MITIGABLE  
IMPACTS ZONE 1

DENOTES MITIGABLE  
IMPACTS ZONE 2



WAKE COUNTY

N.C. DEPT. OF TRANSPORTATION  
DIVISION OF HIGHWAYS

BUFFER







CONST. REVISION : 2/20/04 R2 OF PAVEMENT SCHEDULE CONC. EXPRESSWAY  
GUTTER REVISED TO SHOULDER BERM GUTTER FILE

PAVEMENT SCHEDULE

C1	PROPOSED APPROX. 60 mm ASPHALT CONC. SURFACE COURSE, TYPE S9.5B, AT AN AVERAGE RATE OF 72 kg PER SQ. METER IN EACH OF TWO LAYERS.	J3	PROPOSED 110 mm AGGREGATE BASE COURSE.
C2	PROPOSED VARIABLE DEPTH ASPHALT CONC. SURFACE COURSE, TYPE S9.5B, AT AN AVERAGE RATE OF 2.40 kg PER SQ. METER PER 1 mm DEPTH, TO BE PLACED IN LAYERS NOT LESS THAN 25 mm OR GREATER THAN 40 mm. IN DEPTH.	J4	PROPOSED VARIABLE DEPTH AGGREGATE BASE COURSE.
C3	PROPOSED APPROX. 70 mm ASPHALT CONC. SURFACE COURSE, TYPE S9.5C, AT AN AVERAGE RATE OF 84 kg PER SQ. METER IN EACH OF TWO LAYERS.	K	SUBBASE TO BE TREATED WITH LIME TO A DEPTH OF 200mm, AT A RATE OF 11 KG. PER SQ. METER, AS DIRECTED BY THE ENGINEER. OR SUBBASE TO BE TREATED WITH CEMENT TO A DEPTH OF 180mm, AT A RATE OF 30 KG. PER SQ. METER, AS DIRECTED BY THE ENGINEER. OR SUBBASE TO BE TREATED WITH AGGREGATE AT A RATE OF 135 KG. PER SQ. METER AND CEMENT AT A RATE OF 30 KG. PER SQ. METER TO A DEPTH OF 180mm, AS DIRECTED BY THE ENGINEER.
C4	PROPOSED APPROX. 40 mm ASPHALT CONC. SURFACE COURSE, TYPE S9.5B, AT AN AVERAGE RATE OF 96 kg PER SQ. METER.		
D1	PROPOSED APPROX. 60 mm ASPHALT CONC. BINDER COURSE, TYPE 119.0B, AT AN AVERAGE RATE OF 147 kg PER SQ. METER.	P	PRIME COAT
D2	PROPOSED APPROX. 80 mm ASPHALT CONC. BINDER COURSE, TYPE 119.0C, AT AN AVERAGE RATE OF 196 kg PER SQ. METER.	R1	450 mm CONCRETE CURB AND GUTTER.
D3	PROPOSED APPROX. 110 mm ASPHALT CONC. BINDER COURSE, TYPE 119.0C, AT AN AVERAGE RATE OF 269.5 kg PER SQ. METER.	R2	CONCRETE EXPRESSWAY GUTTER.
E1	PROPOSED APPROX. 200 mm ASPHALT CONC. BASE COURSE, TYPE B25.0C, AT AN AVERAGE RATE OF 245 kg PER SQ. METER IN EACH OF TWO LAYERS.	R3	125 mm MONOLITHIC CONCRETE ISLAND.
E2	PROPOSED VARIABLE DEPTH ASPHALT CONC. BASE COURSE, TYPE B25.0B, AT AN AVERAGE RATE OF 2.45 kg PER SQ. METER PER 1 mm DEPTH, TO BE PLACED IN LAYERS NOT LESS THAN 75 mm IN DEPTH OR GREATER THAN 140 mm IN DEPTH.	T	EARTH MATERIAL.
E3	PROPOSED APPROX. 100 mm ASPHALT CONC. BASE COURSE, TYPE B25.0B, AT AN AVERAGE RATE OF 245 kg PER SQ. METER.	U	EXISTING PAVEMENT.
J1	PROPOSED 200 mm AGGREGATE BASE COURSE.	V	INCIDENTAL MILLING ASPHALT PAVEMENT VARIABLE DEPTH.
J2	PROPOSED 250 mm AGGREGATE BASE COURSE.	W	VARIABLE DEPTH ASPHALT PAVEMENT. (SEE STANDARD WEDGING DETAIL)

NOTE: PAVEMENT EDGE SLOPES ARE 1:1 UNLESS SHOWN OTHERWISE.

TYPICAL SECTION NO. 1

FDPS = FULL DEPTH PAVED SHOULDERS

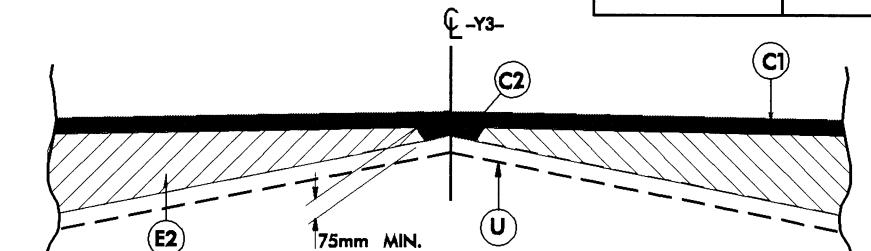
USE T.S. NO. 1 IN THE FOLLOWING LOCATIONS:

L - STA. 34+80.519 TO BEGIN BRIDGE STA. 35+22.727

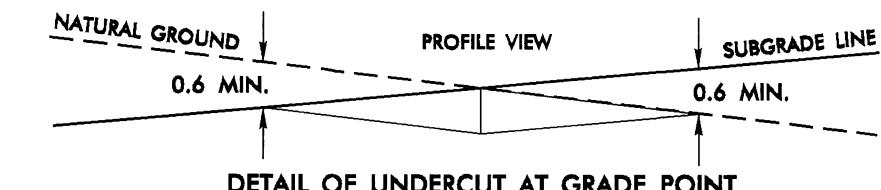
L - END BRIDGE STA. 35+70.713 TO BEGIN BRIDGE STA. 38+23.750

PROJECT REFERENCE NO. R-28098 SHEET NO. 2

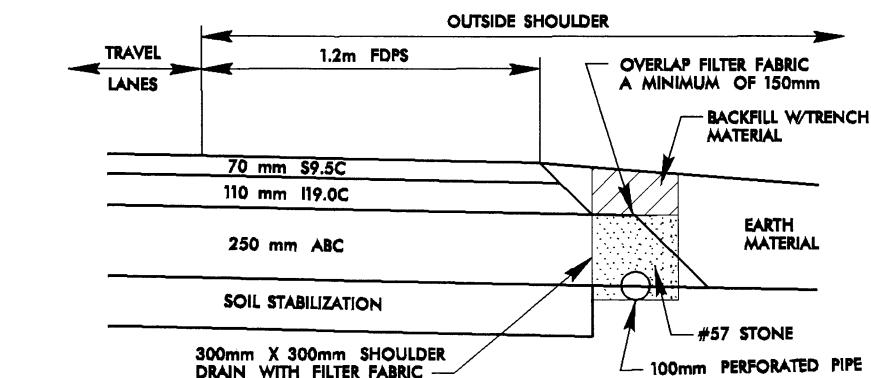
ROADWAY DESIGN ENGINEER PAVEMENT DESIGN ENGINEER



DETAIL SHOWING METHOD OF WEDGING NO. 1

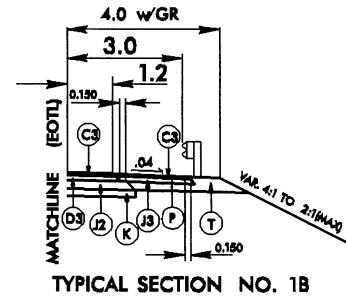
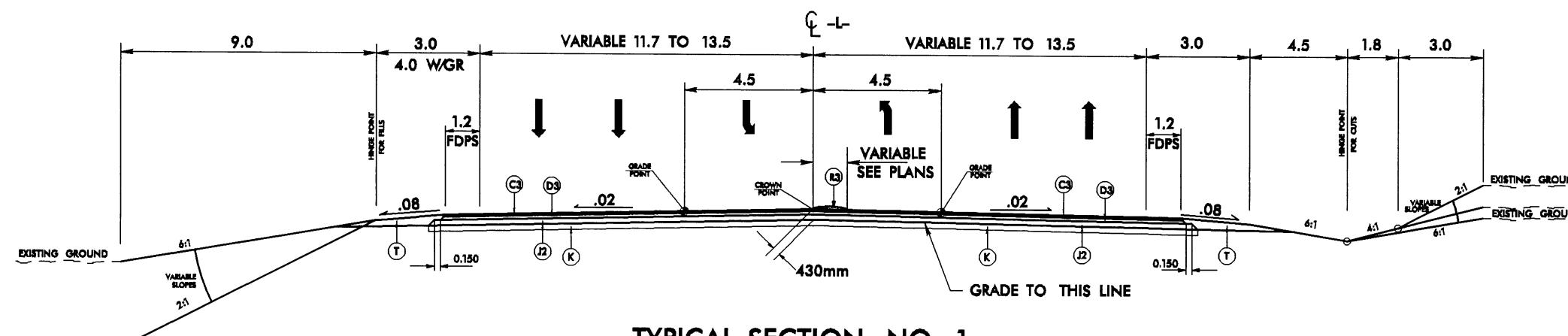


DETAIL OF UNDERCUT AT GRADE POINT

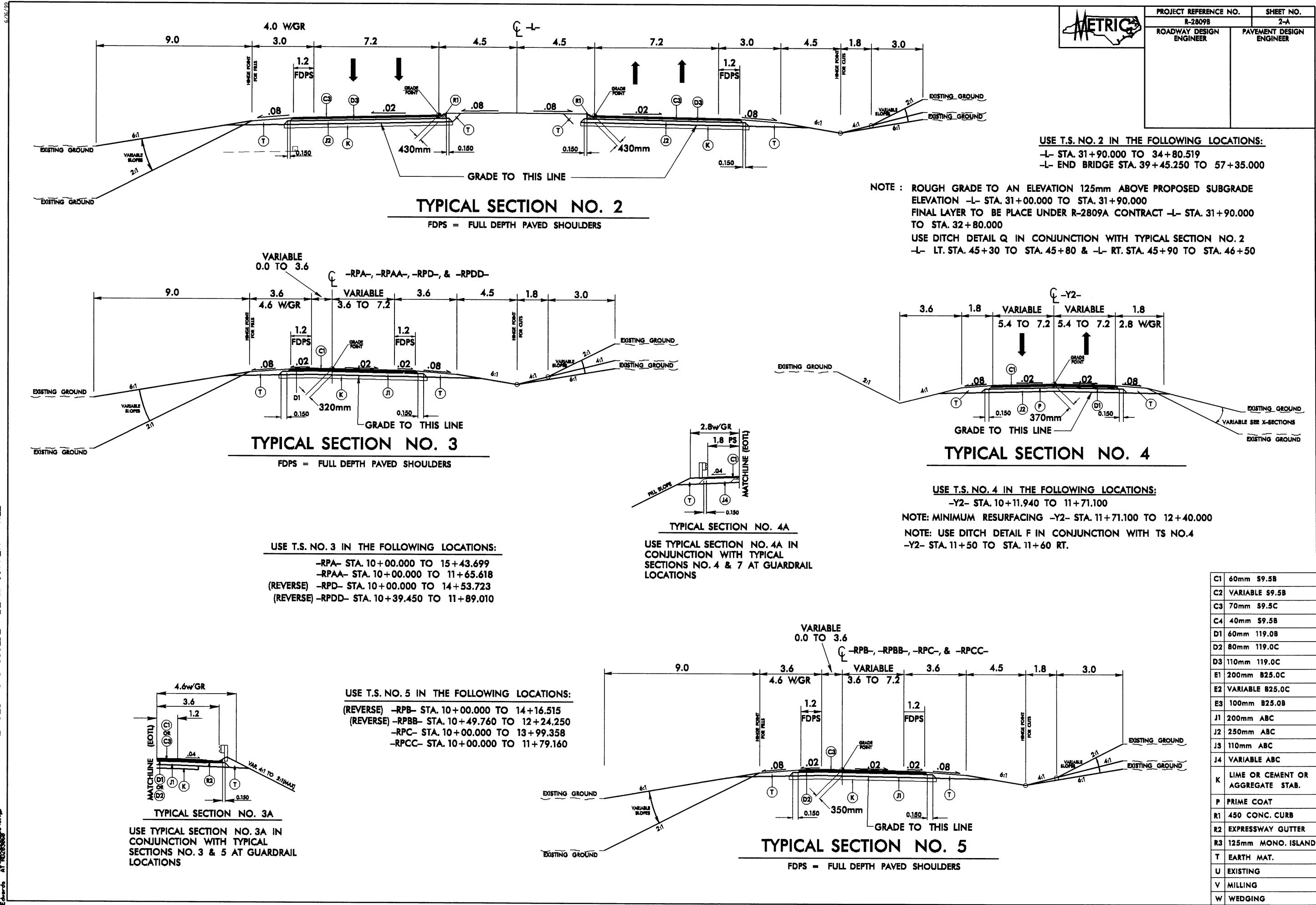


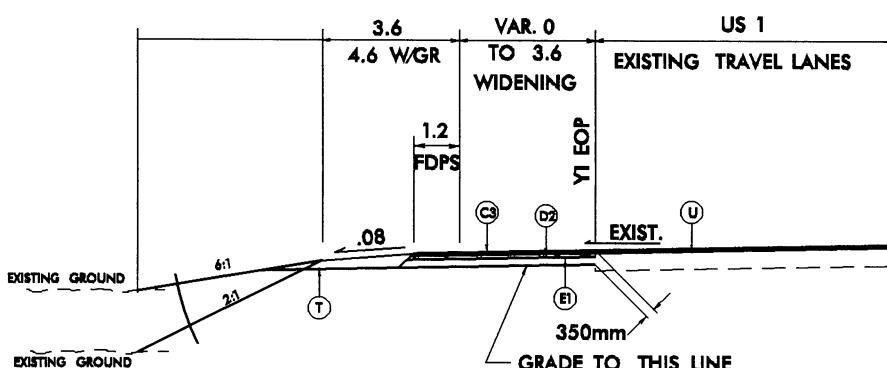
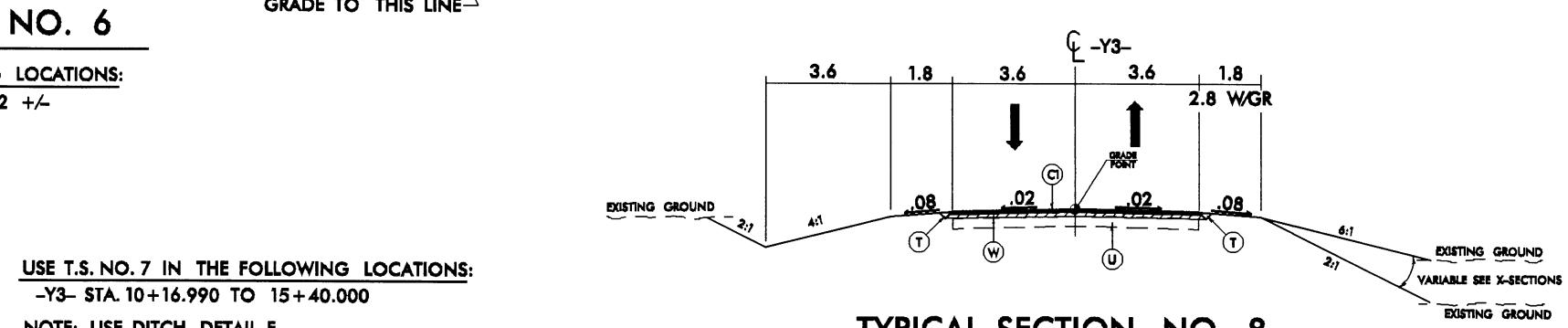
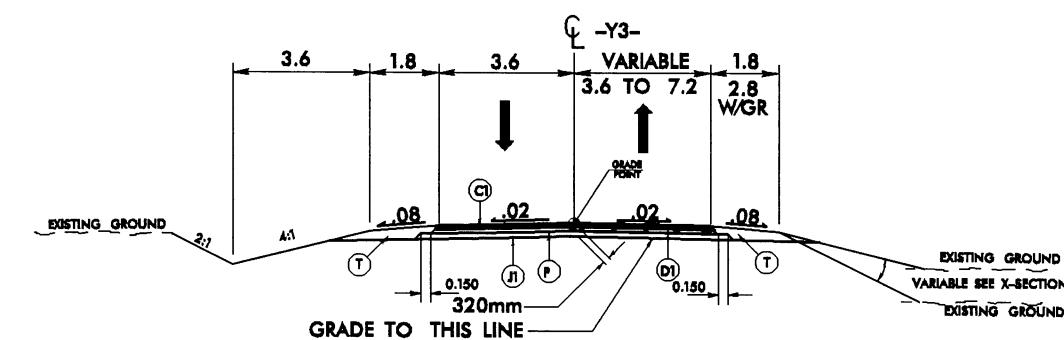
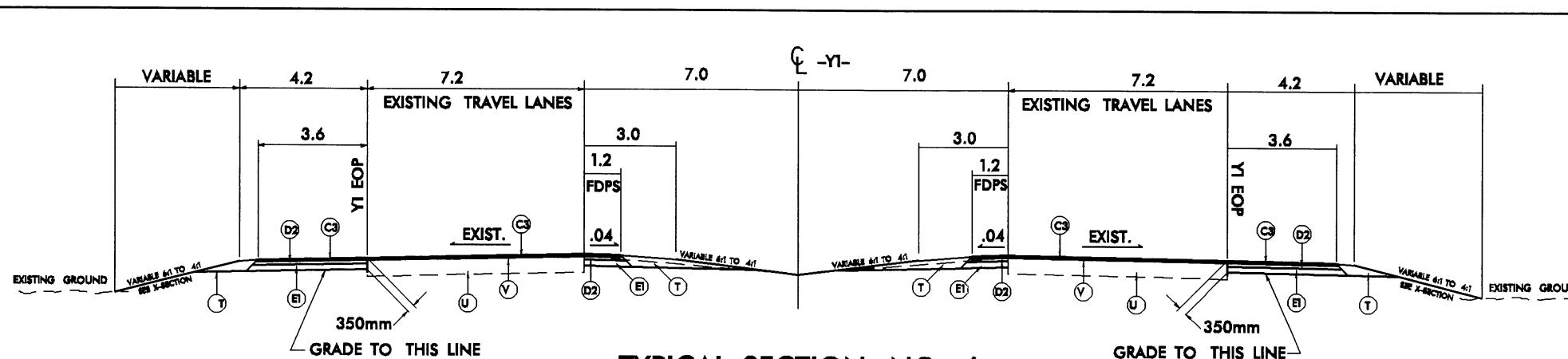
SHOULDER DRAIN DETAIL

NOTE : ALL OUTLET PIPES SHALL USE A 1% GRADE  
USE IN CONJUNCTION WITH TYPICAL SECTION NO.s 1 & 2



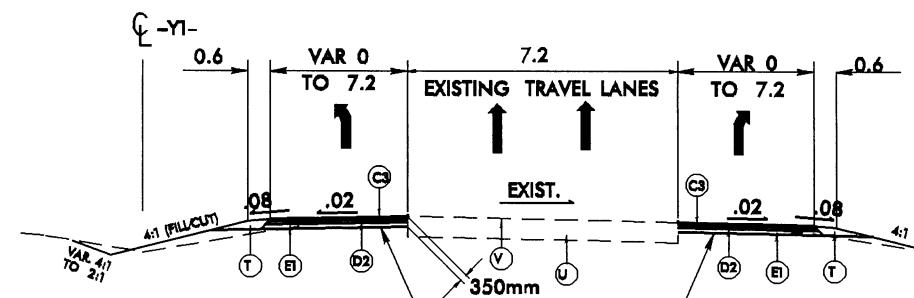
USE TYPICAL SECTION NO. 1B IN CONJUNCTION WITH TYPICAL SECTIONS NO. 1 & 2 AT GUARDRAIL LOCATIONS





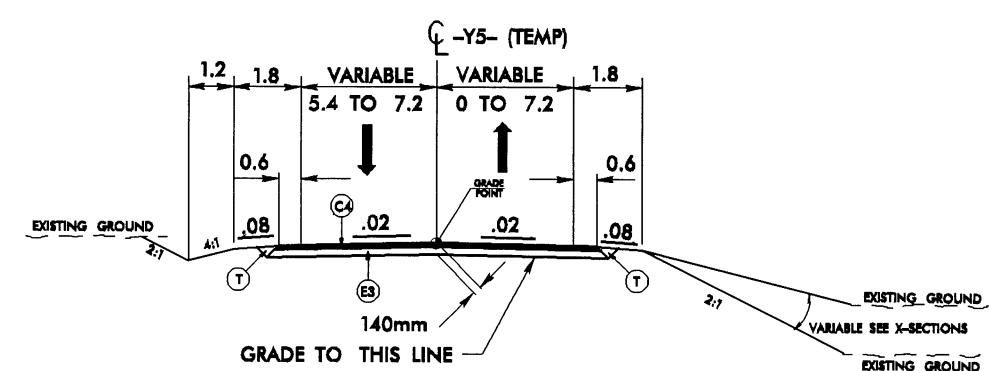
USE T.S. NO. 9 IN CONJUNCTION WITH T.S. NOS 3 & 6:  
 LT. -Y1- STA. 16+23.559 TO 17+82.508  
 (REVERSE) RT. -Y1- STA. 27+60.000 TO 28+11.528  
 LT. -Y1- STA. 16+90.343 TO 17+80.350  
 (REVERSE) RT. -Y1- STA. 26+82.111 TO 28+32.111

NOTE: STATION RANGES INCLUDE TAPERS



USE T.S. NO. 10 IN THE FOLLOWING LOCATIONS:  
 -Y1- STA. 20+81 TO 21+47 (NBL MED.)  
 -Y1- STA. 24+57 TO 25+60 (NBL MED.)  
 -Y1- STA. 25+90 TO 27+50 (SBL MED.)  
 -Y1- STA. 25+92 TO 26+37 (SBL OUTSIDE)

USE T.S. NO. 11 IN THE FOLLOWING LOCATIONS:  
 -Y5- STA. 10+64.044 TO 11+01.402  
 -Y5- STA. 11+08.643 TO 11+22.630  
 -Y5- STA. 11+36.904 TO 11+54.497  
 -Y5- STA. 11+65.620 TO 11+84.147 (WIDENING RT. SIDE ONLY)



SEE TRAFFIC CONTROL PLANS TCP-13 & 2-V

C1	60mm \$9.5B
C2	VARIABLE \$9.5B
C3	70mm \$9.5C
C4	40mm \$9.5B
D1	60mm I19.0B
D2	80mm I19.0C
D3	110mm I19.0C
E1	200mm B25.0C
E2	VARIABLE B25.0C
E3	100mm B25.0B
J1	200mm ABC
J2	250mm ABC
J3	110mm ABC
J4	VARIABLE ABC
K	LIME OR CEMENT OR AGGREGATE STAB.
P	PRIME COAT
R1	450 CONC. CURB
R2	EXPRESSWAY GUTTER
R3	125mm MONO. ISLAND
T	EARTH MAT.
U	EXISTING
V	MILLING
W	WEDGING

# CURVE DATA SHEET



PROJECT REFERENCE NO.		SHEET NO.
R-2809B		2-C
ROADWAY DESIGN ENGINEER		
THIS DOCUMENT ORIGINALLY ISSUED AND SEALED BY RONALD D. ALLEN, PE, 15356 ON AUGUST 22, 2003		

Pls Sta 29+80.149 $\theta_s = 4^{\circ}38'30''$ $L_s = 64.000$ $L_T = 42.681$ $S_T = 21.347$	Pls Sta 30+72.330 $\Delta = 20^{\circ}20'27.8'' (LT)$ $L_s = 140.232$ $T = 70.862$ $R = 395.000$ $SE = SEE PLANS$ $V = 100 \text{ km/h}$	Pls Sta 31+63.047 $\theta_s = 4^{\circ}38'30.5''$ $L_s = 64.000$ $L_T = 42.681$ $S_T = 21.347$	Pls Sta 39+80.278 $\theta_s = 1^{\circ}22'37.4''$ $L_s = 56.000$ $L_T = 37.334$ $S_T = 18.668$	Pls Sta 41+80.849 $\Delta = 17^{\circ}44'57.4'' (LT)$ $L_s = 360.898$ $T = 181.906$ $R = 1165.000$ $SE = SEE PLANS$ $V = 100 \text{ km/h}$	Pls Sta 43+78.509 $\theta_s = 1^{\circ}22'37.4''$ $L_s = 56.000$ $L_T = 37.334$ $S_T = 18.668$	Pls Sta 51+49.627 $\Delta = 30^{\circ}16'49'' (RT)$ $L_s = 1.231.384$ $T = 630.434$ $R = 2.330.000$ $SE = SEE PLANS$ $V = 100 \text{ km/h}$
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-Y1-

Pls Sta 16+96.995 $\Delta = 21^{\circ}27'04.2'' (RT)$ $L_s = 655.189$ $T = 331.475$ $R = 1750.000$ $SE = SEE PLANS$	Pls Sta 20+40.708 $\theta_s = 0^{\circ}58'56.0''$ $L_s = 60.000$ $L_T = 40.001$ $S_T = 20.001$
--	--

-RPA-

Pls Sta 14+81.874 $\theta_s = 15^{\circ}54'55.5''$ $L_s = 50.000$ $L_T = 33.469$ $S_T = 16.790$	Pls Sta 15+58.228 $\Delta = 67^{\circ}13'28.7'' (LT)$ $L_s = 50.000$ $T = 59.824$ $ST = 16.790$	Pls Sta 16+207.91 $\theta_s = 15^{\circ}54'55.8''$ $L_s = 50.000$ $L_T = 33.469$ $ST = 16.790$
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-RPAA-

Pls Sta 10+48.900 $\theta_s = 4^{\circ}20'26.5''$ $L_s = 50.000$ $L_T = 33.343$ $S_T = 16.676$	Pls Sta 11+13.710 $\Delta = 16^{\circ}36'13.6'' (RT)$ $L_s = 95.631$ $T = 48.153$ $R = 330.000$ $SE = SEE PLANS$ $V = 50 \text{ km/h}$
--	--

-RPB-

Pls Sta 10+27.308 $\theta_s = 0^{\circ}48'42.5''$ $\theta_s = 1^{\circ}25'56.7''$ $L_s = 50.000$ $L_T = 27.308$ $S_T = 22.699$	Pls Sta 10+65.364 $\Delta = 4^{\circ}03'02.8'' (LT)$ $L_s = 70.699$ $R = 1.000.000$ $SE = SEE PLANS$ $V = 100 \text{ km/h}$	Pls Sta 11+37.367 $\theta_s = 1^{\circ}25'56.6''$ $L_s = 50.000$ $L_T = 33.334$ $S_T = 16.668$	Pls Sta 12+92.240 $\theta_s = 13^{\circ}01'18.4''$ $L_s = 50.000$ $L_T = 33.424$ $ST = 16.749$	Pls Sta 13+93.848 $\Delta = 75^{\circ}24'33.2'' (RT)$ $L_s = 144.775$ $T = 105.032$ $R = 110.000$ $SE = SEE PLANS$ $V = 50 \text{ km/h}$	Pls Sta 14+70.340 $\theta_s = 13^{\circ}01'18.4''$ $L_s = 50.000$ $L_T = 33.424$ $ST = 16.749$
---	--	--	--	--	--

-RPBB-

Pls Sta 11+91.040 $\theta_s = 15^{\circ}54'55.8''$ $L_s = 50.000$ $L_T = 33.469$ $ST = 16.790$	Pls Sta 11+39.737 $\Delta = 46^{\circ}42'58.6'' (LT)$ $L_s = 73.382$ $T = 38.868$ $R = 90.000$ $SE = SEE PLANS$ $V = 50 \text{ km/h}$	Pls Sta 10+84.337 $\theta_s = 15^{\circ}54'55.8''$ $L_s = 50.000$ $L_T = 33.469$ $ST = 16.790$
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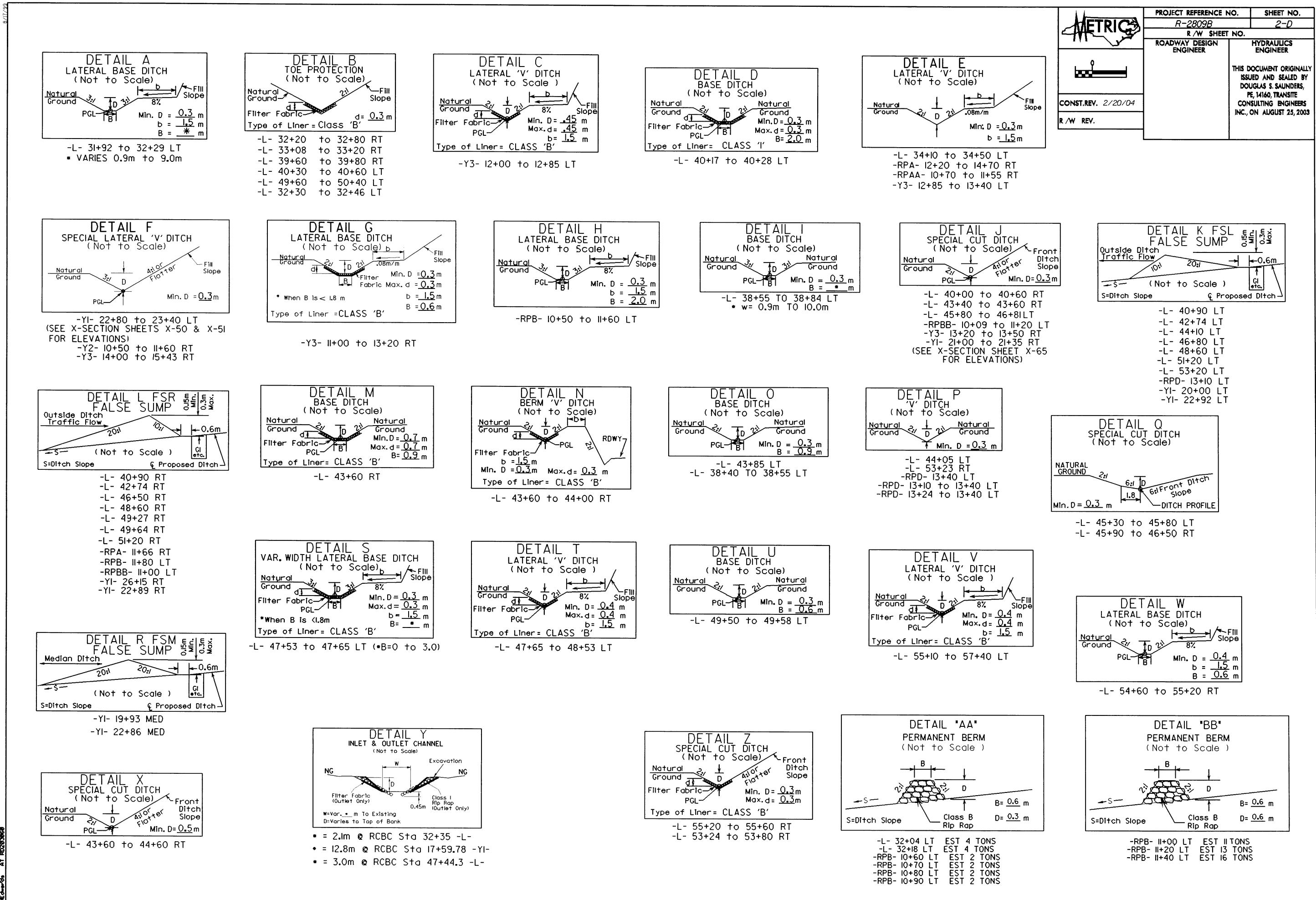
-RPC-

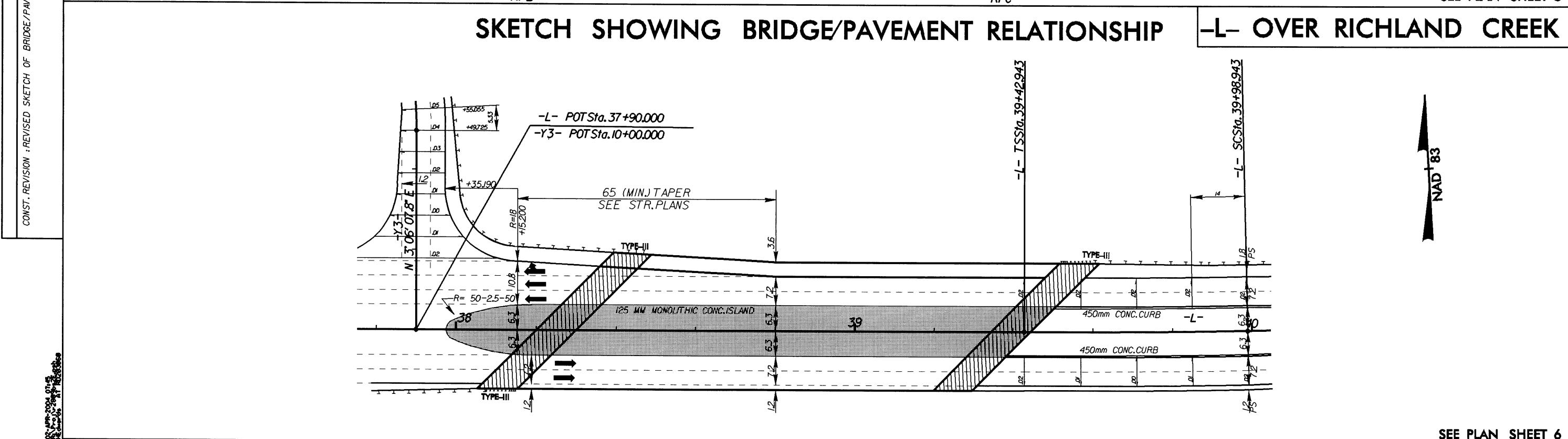
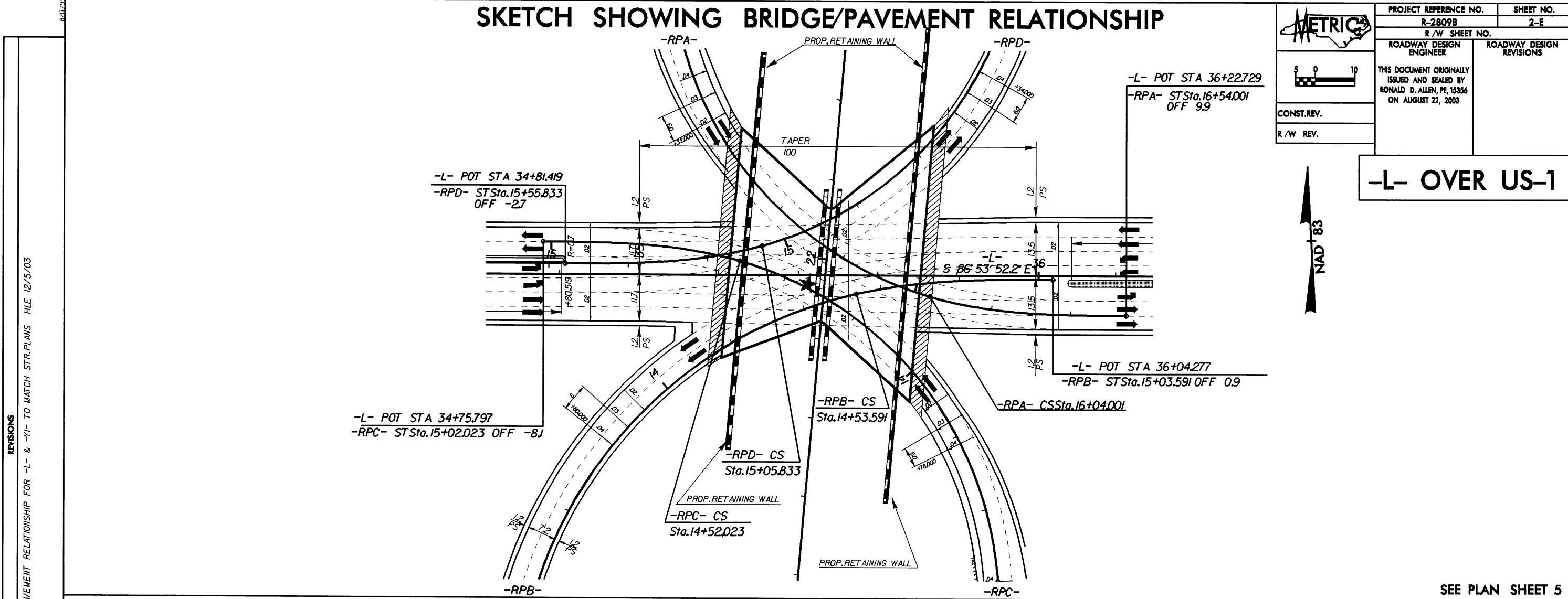
Pls Sta 10+33.338 $\theta_s = 2^{\circ}51'53.2''$ $L_s = 50.000$ $L_T = 33.338$ $S_T = 16.671$	Pls Sta 10+88.964 $\Delta = 8^{\circ}54'42.8'' (RT)$ $L_s = 77.771$ $T = 38.964$ $R = 500.000$ $SE = SEE PLANS$ $V = 100 \text{ km/h}$	Pls Sta 11+44.442 $\theta_s = 2^{\circ}51'53.2''$ $L_s = 50.000$ $L_T = 33.338$ $ST = 16.671$	Pls Sta 13+24.887 $\theta_s = 15^{\circ}54'55.8''$ $L_s = 50.000$ $L_T = 33.469$ $ST = 16.790$	Pls Sta 14+04.922 $\Delta = 70^{\circ}24'49.0'' (LT)$ $L_s = 110.605$ $T = 63.504$ $R = 90.000$ $SE = SEE PLANS$ $V = 50 \text{ km/h}$	Pls Sta 14+68.813 $\theta_s = 15^{\circ}54'55.8''$ $L_s = 50.000$ $L_T = 33.469$ $ST = 16.790$
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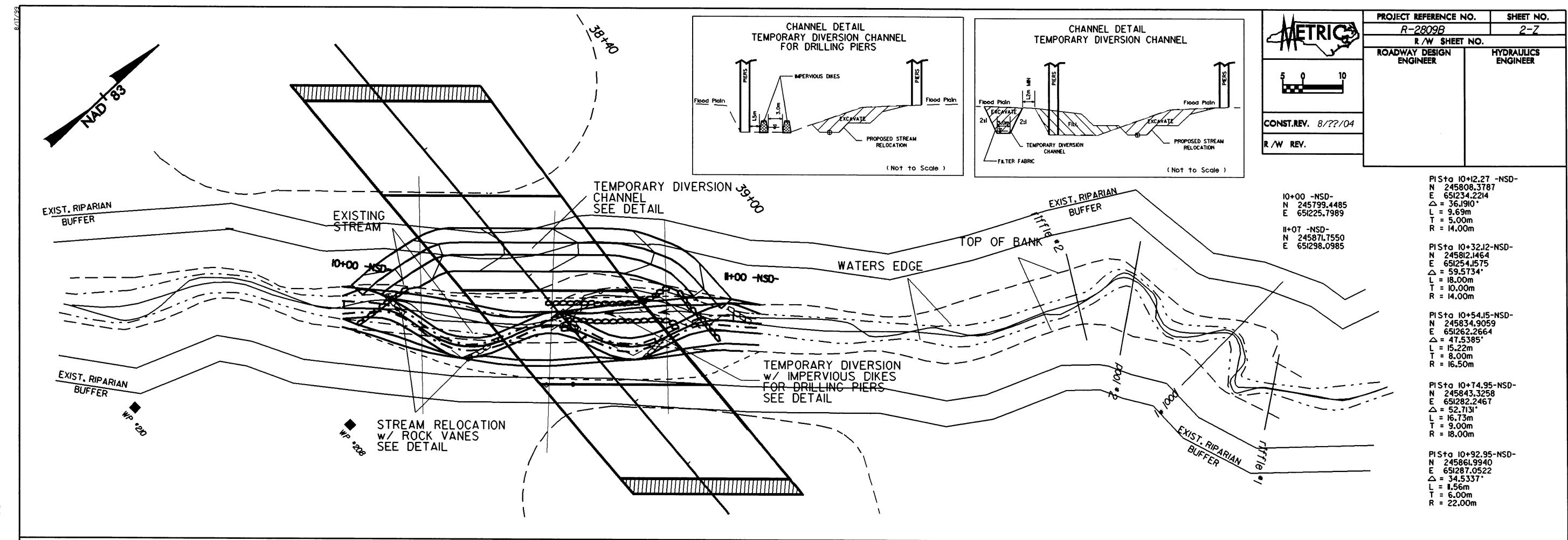
-RPCC-

Pls Sta 10+50.573 $\Delta = 11^{\circ}33'03.9'' (RT)$ $L_s = 100.802$ $T = 50.573$ $R = 500.000$ $SE = 0.03$ $V = 50 \text{ km/h}$
--

-RPD-







STREAM DETAIL

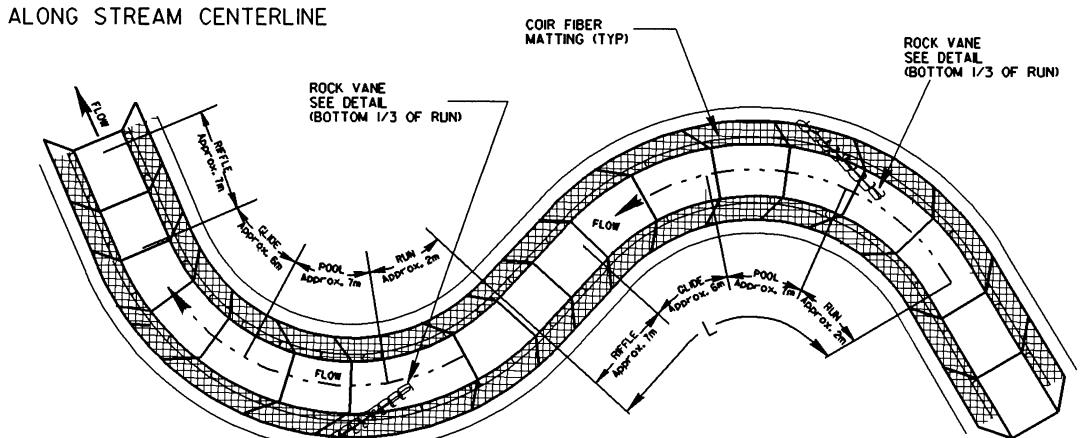
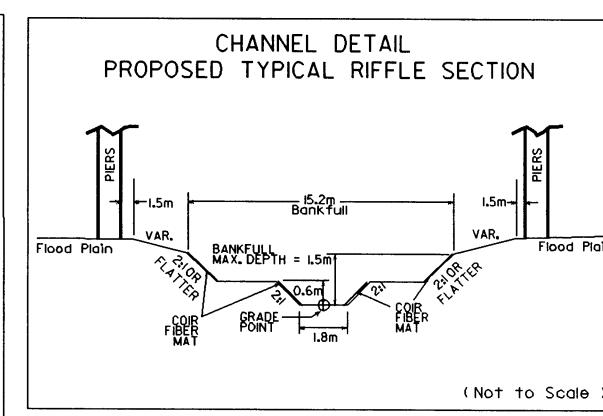
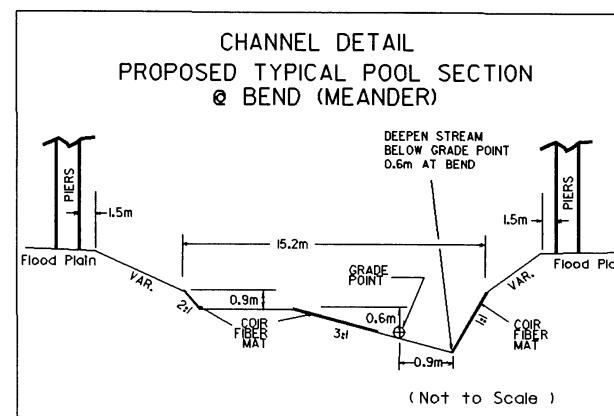
L = LENGTH ALONG STREAM CENTERLINE

## QUANTITIES: (Temp. Diversions)

FILTER FABRIC = 1000 sq.m.  
EXCAVATION = 1900 cu.m.

## QUANTITIES

COIR FIBER MAT = 750 sq.m.  
EXCAVATION = 900 cu.m.



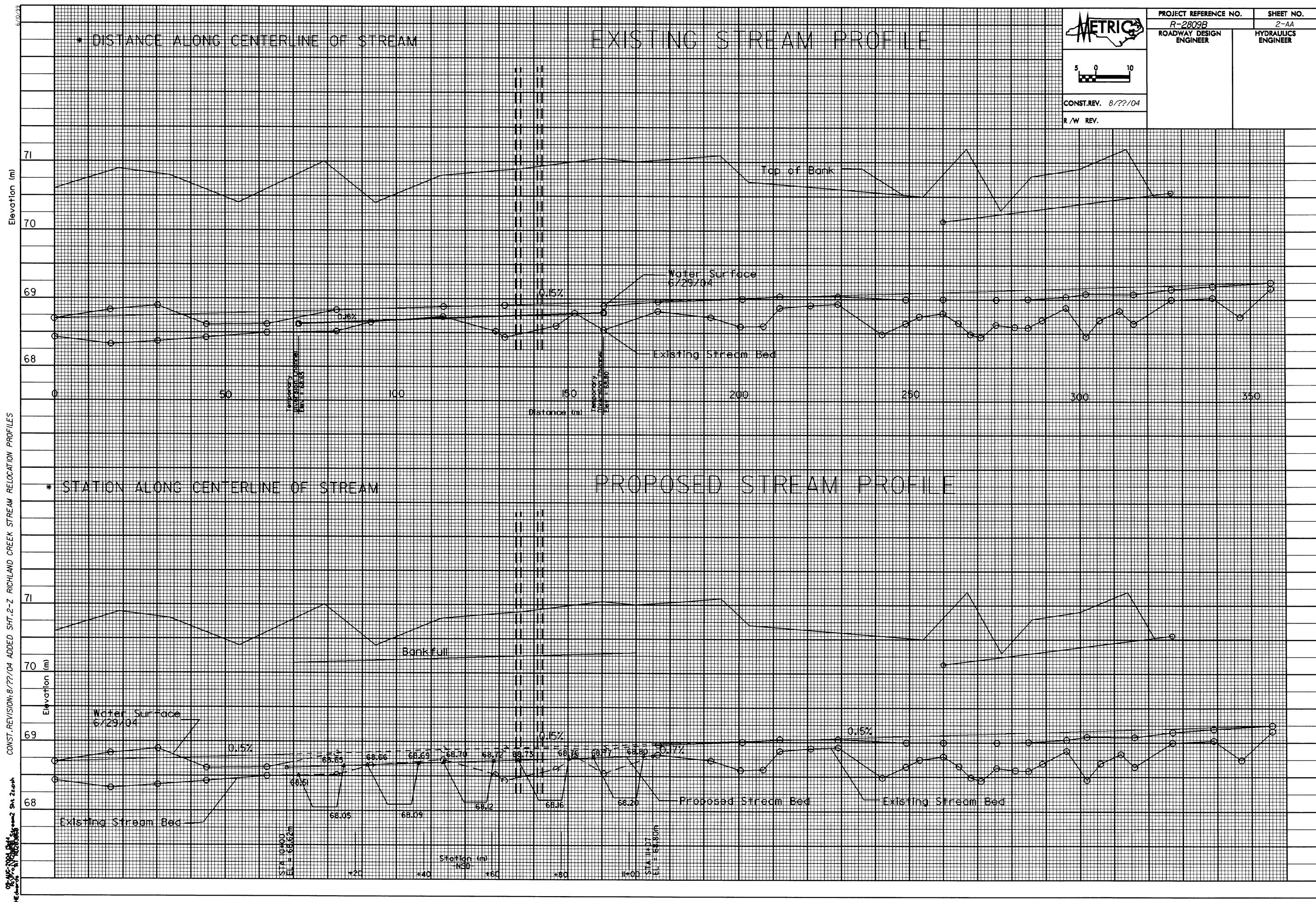
## NOTES

PLANTINGS SHOULD BE PLACED ABOVE BANKFULL DEPTH.

ROCK VANES TO BE PLACED IN BOTTOM ONE THIRD OF RUN

ROCK SHOULD BE OBLONG IN SHAPE AND HAVE MINIMUM DIMENSIONS OF 0.9mX0.6mX0.6m  
(SEE ROCK VANE DETAIL.)

**NCDOT  
DIVISION OF HIGHWAYS  
WAKE COUNTY  
PROJECT: 8.1402501 (R-2809B)  
NC 98 WAKE FOREST BYPASS  
SHEET OF**



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\* X-SECTIONS SHOWN PERPENDICULAR TO BANKFULL CHANNEL

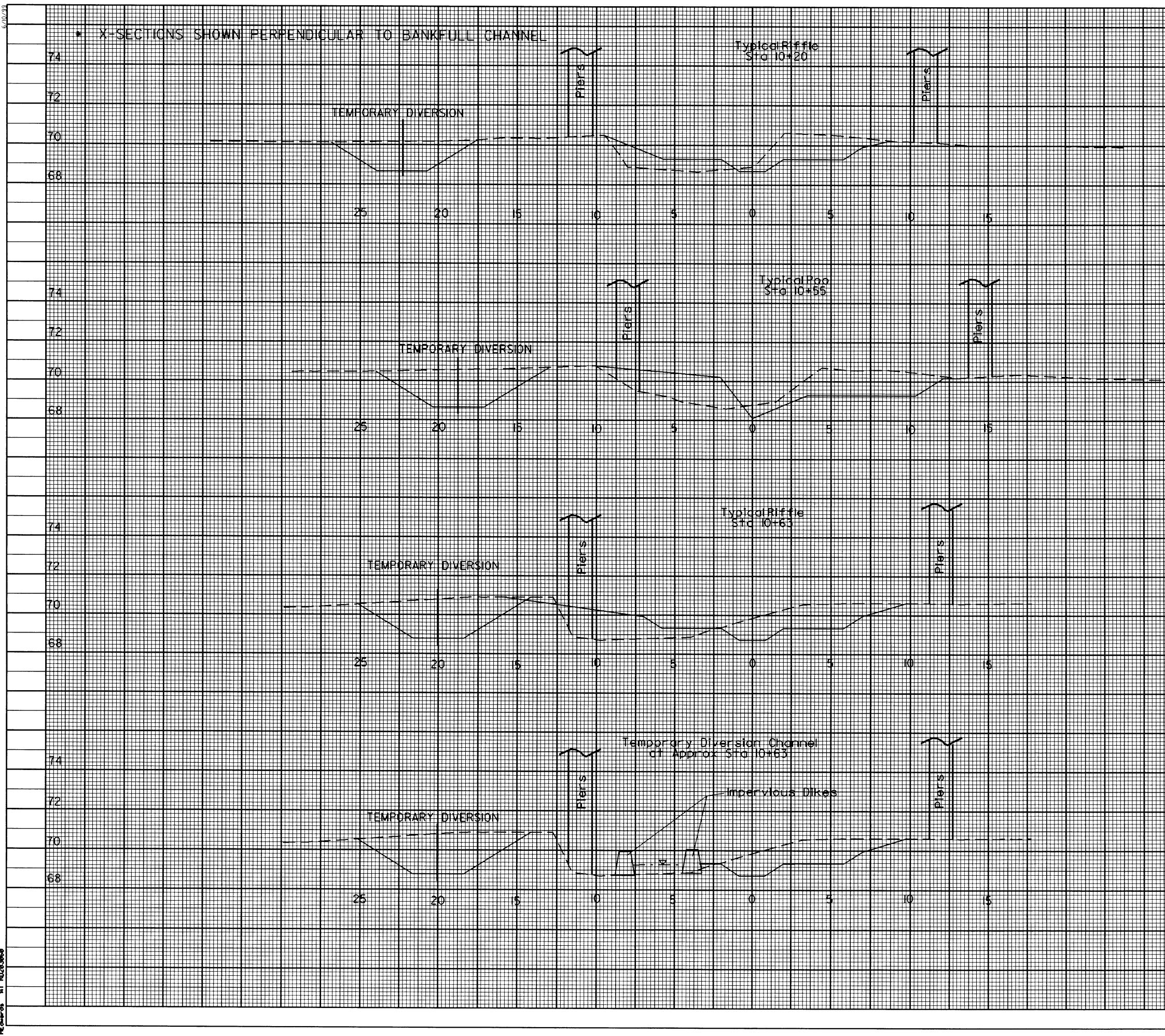
## Typical Riff file Sta 10+20

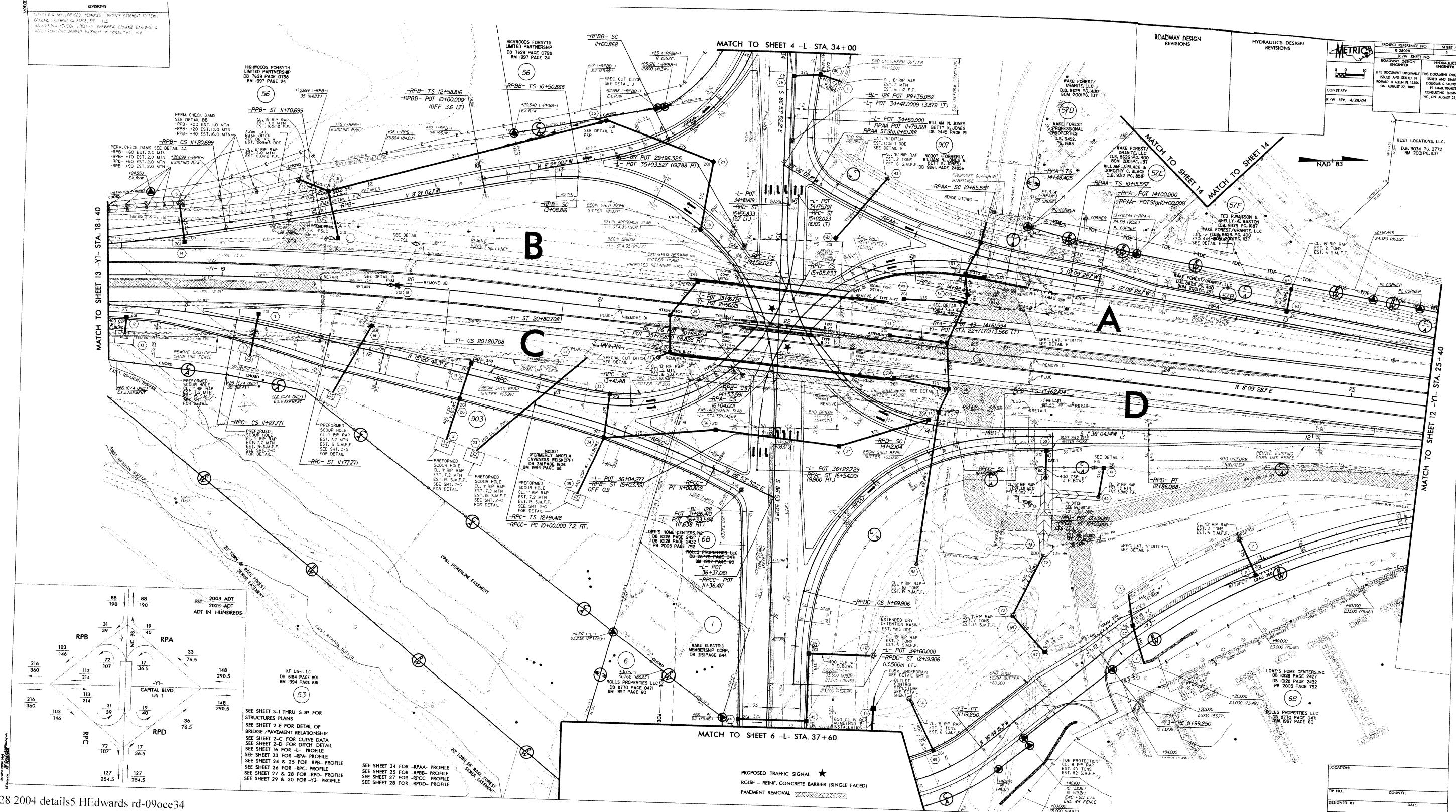
## PROJECT R

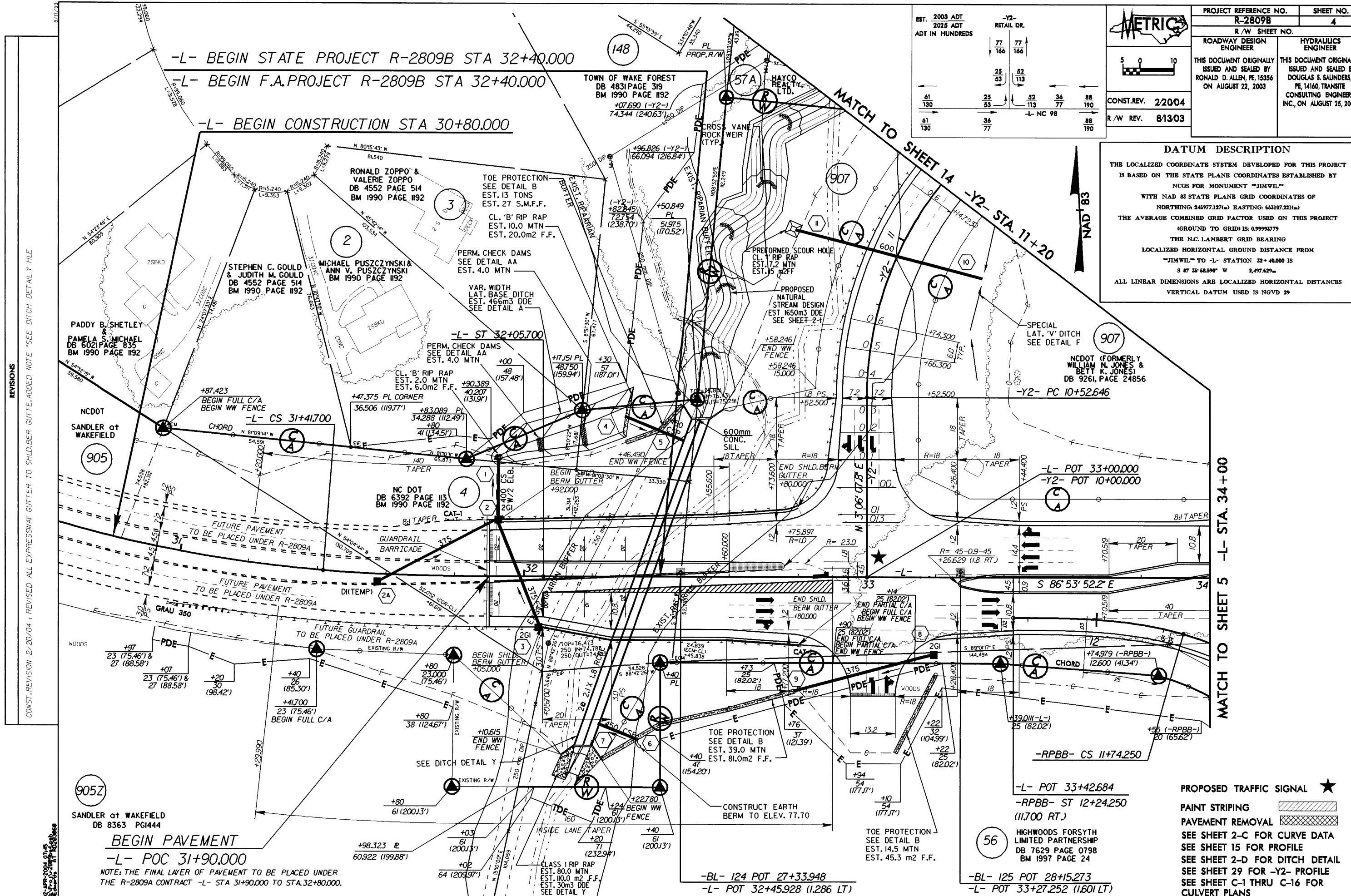
REFERENCE NO.	SHEET NO.
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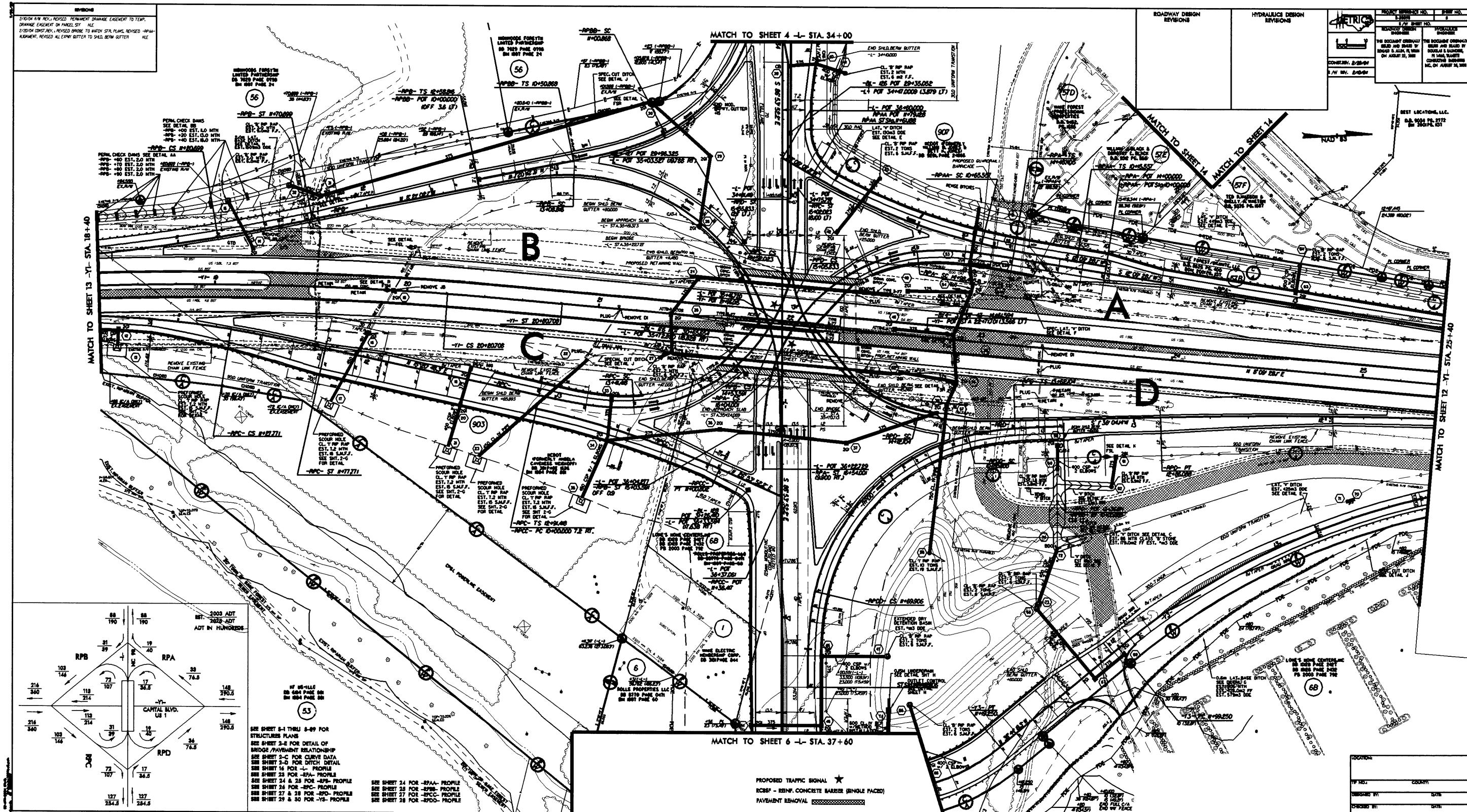
R-28C

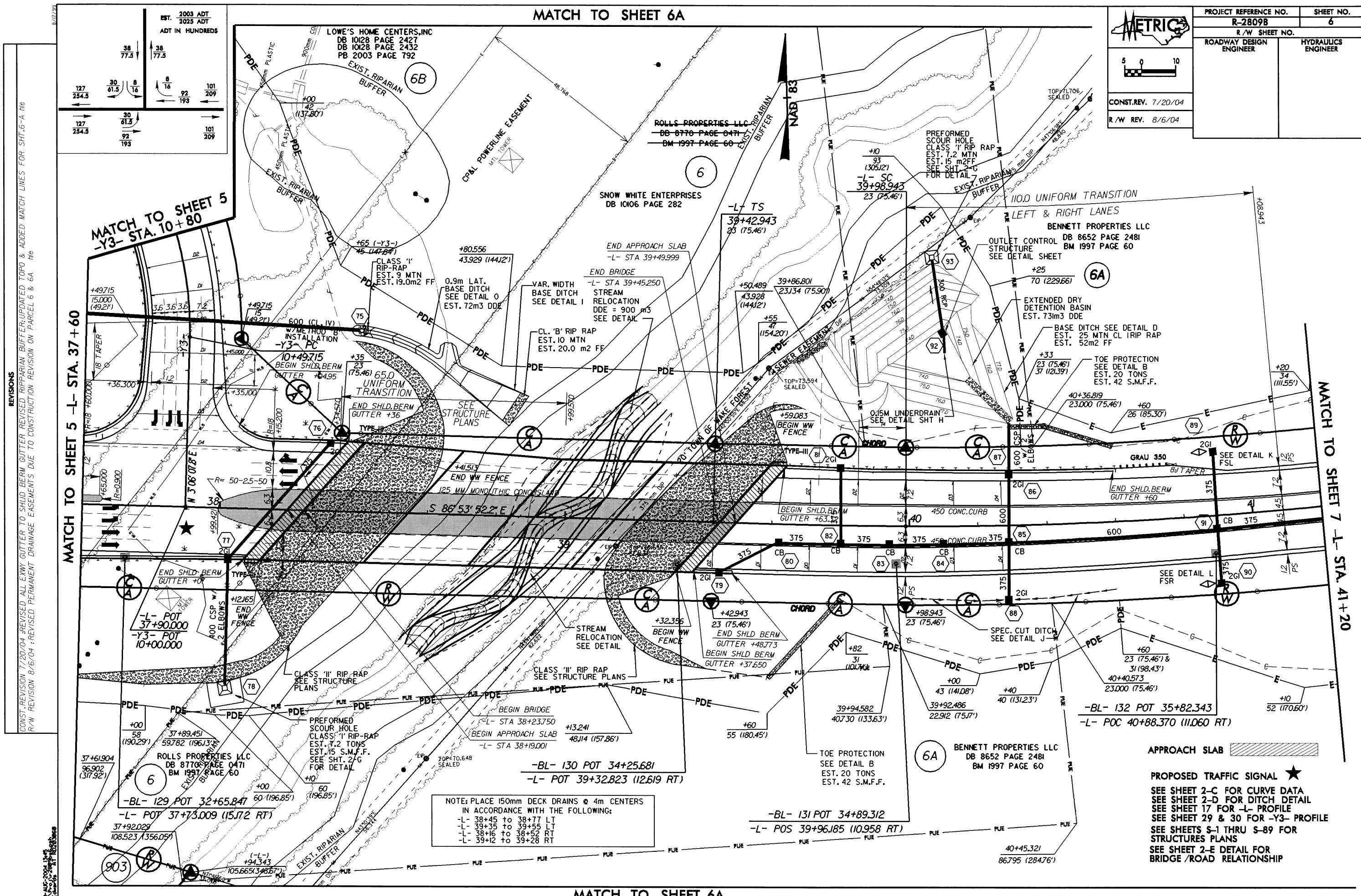
**SHEET NO.**  
**2-BB**





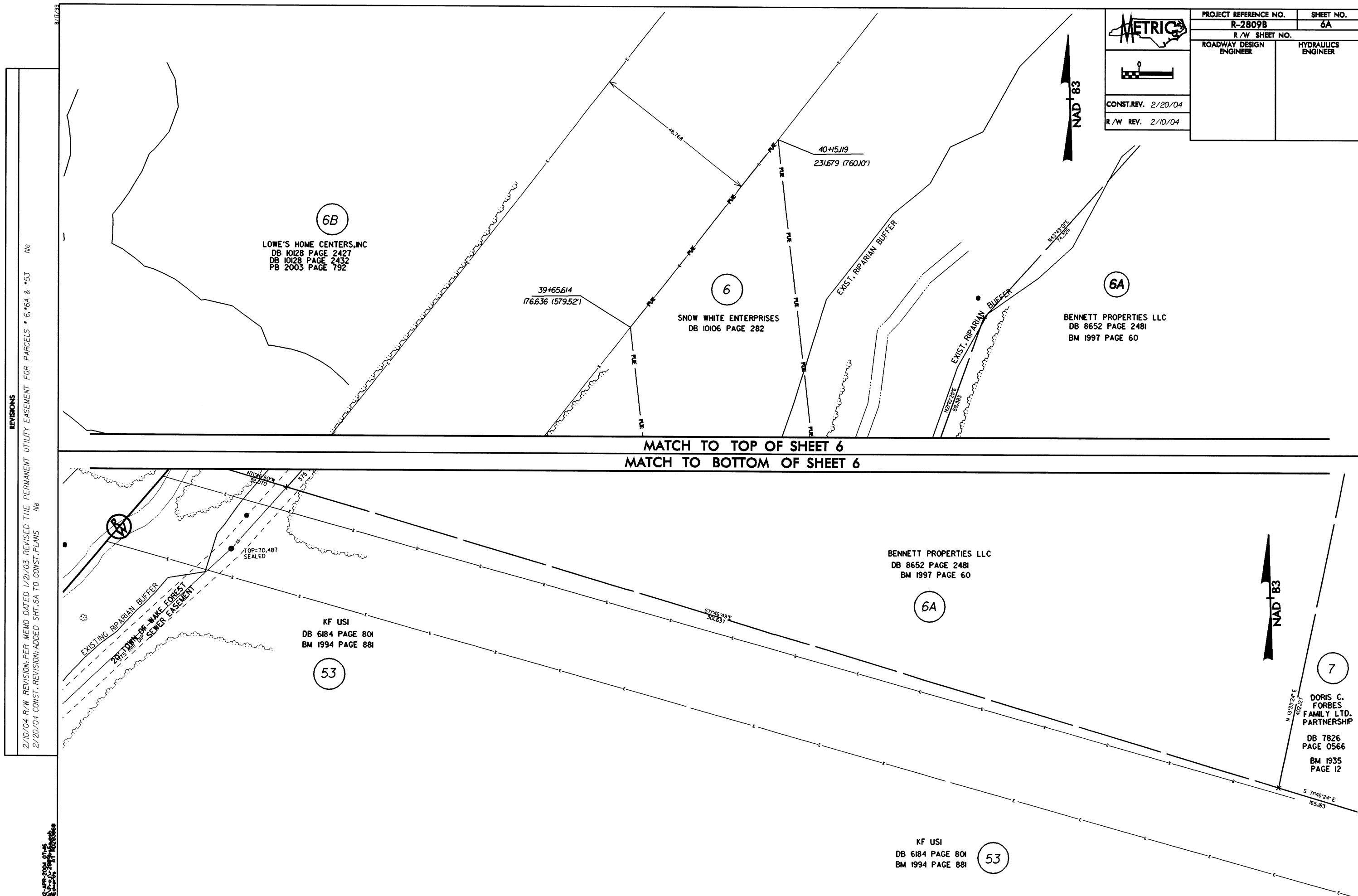


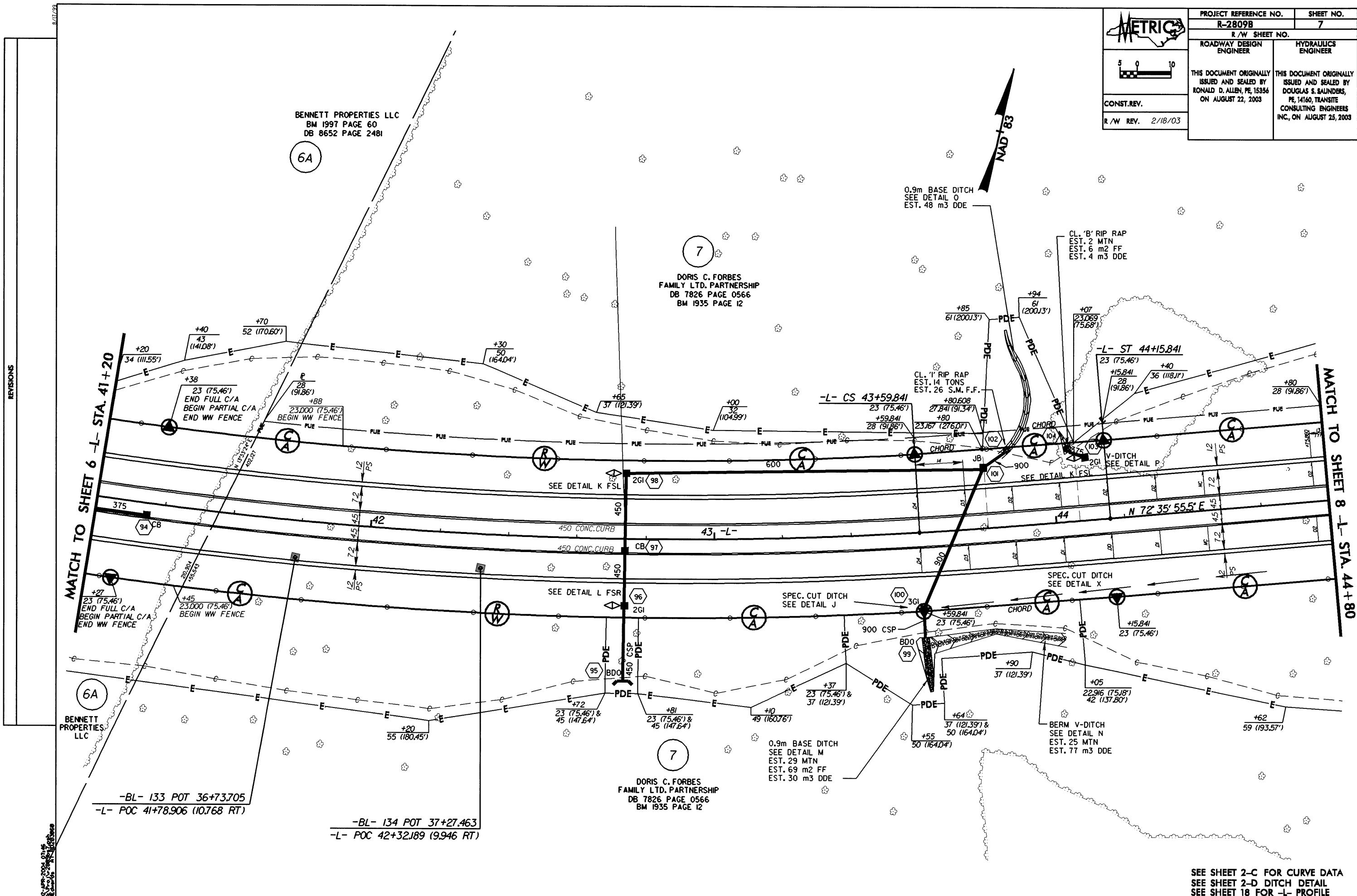




**REVISIONS**  
2/10/04 RW REVISION: PER MEMO DATED 1/21/03 REVISED THE PERMANENT UTILITY EASEMENT FOR PARCELS # 6, 6A & 53  
2/20/04 CONST. REVISION: ADDED SHT.6A TO CONST. PLANS  
he

REVIEWS



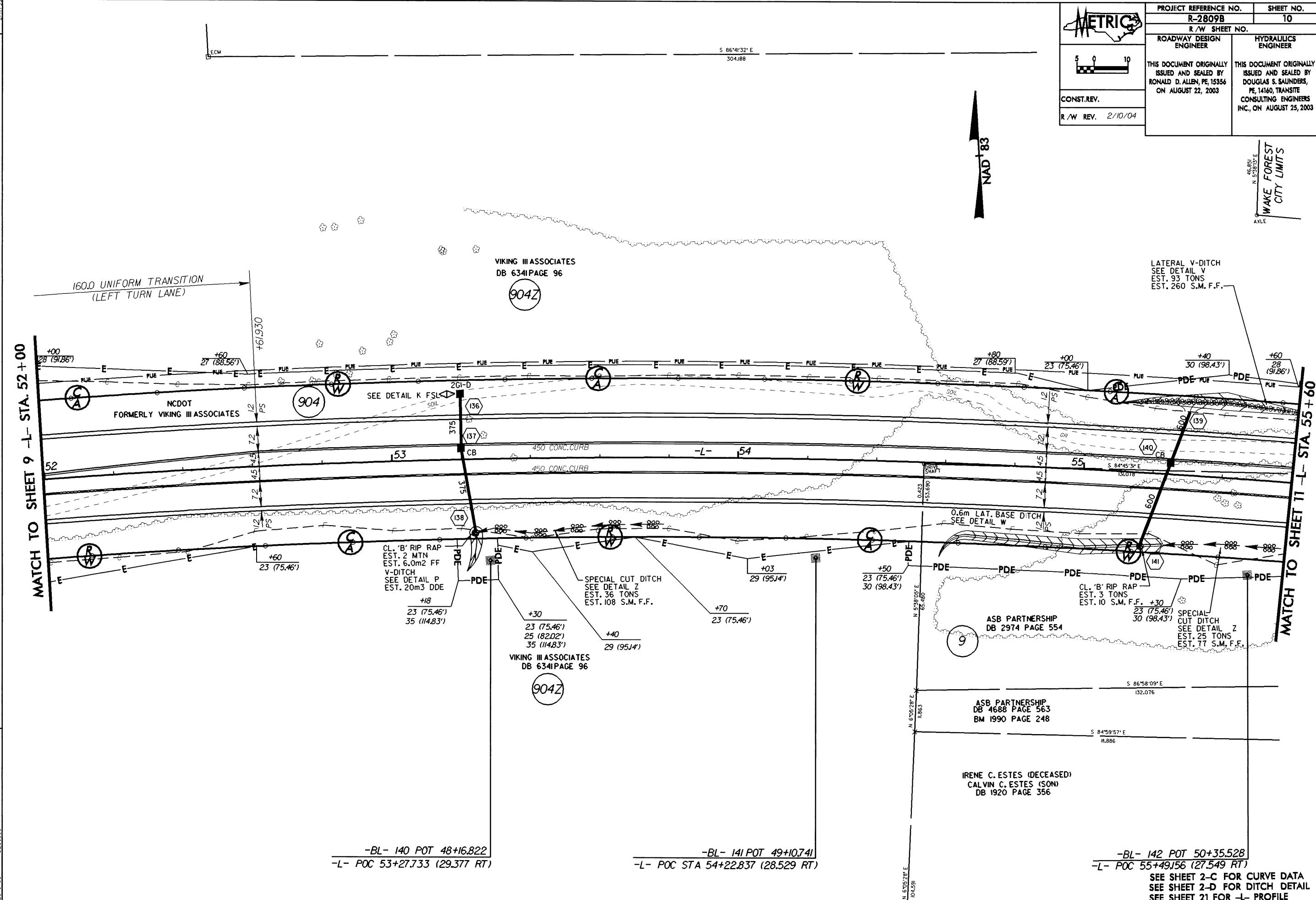






REVISIONS

2/10/04 R/W REVISION: REVISED THE PROPERTY OWNER NAME ON PARCEL • 9

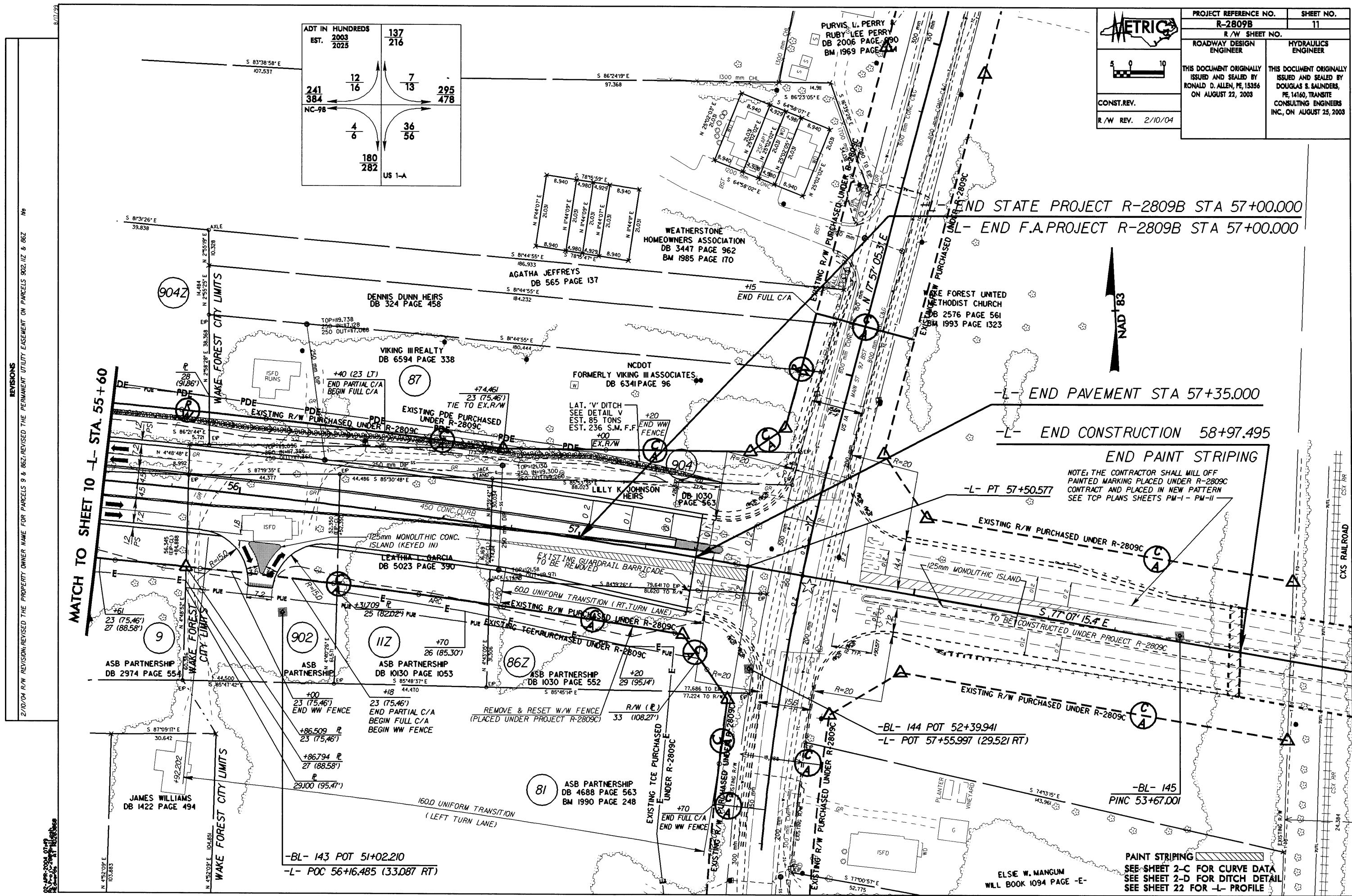


REVISIONS

2/10/04 R/W REVISION; REVISED THE PROPERTY OWNER NAME FOR PARCELS 9 & 8&Z;REVISED THE PERMANENT UTILITY EASEMENT ON PARCELS 9&Z, 11Z & 8&Z

REVISEONS

MATCH TO SHEET 10 - STA. 55±40





MATCH TO SHEET 5 -YI= SIA. 18+40

 	PROJECT REFERENCE NO.	
	<b>R-2809B</b>	
	R /W SHEET NO.	
<b>Roadway Design Engineer</b>  THIS DOCUMENT ORIGINALLY ISSUED AND SEALED BY RONALD D. ALLEN, PE, 15356 ON AUGUST 22, 2003	<b>HYDRAULICS Engineer</b>	
	THIS DOCUMENT ORIGINALLY ISSUED AND SEALED BY DOUGLAS S. SAUNDERS, PE, 14160, TRANSITE CONSULTING ENGINEERS INC., ON AUGUST 25, 2003	
T.REV. 2/20/04		
REV. 2/3/03		

REVISI観

2/20/03 CONST. REVISION: REVISED ALL EXPRESSWAY GUTTER TO SHLD.BERM GUTTER *me*

